

Experiencias en:

Sistemas Interconectados de Alta Tension AC & DC

1

INTRODUCCION: Parametros Linea Transmision, Limites de Operacion, Impedacias Caract. Z_c & SIL

2

Interrupcion Mecanica & Dinamica Electronica de Potencia- Flex. AC (FACTS)

3

Compensacion Shunt, Series & Transformadores \neq Desfase

4

Conversion Sistemas Trifasico a Hexafasico

5

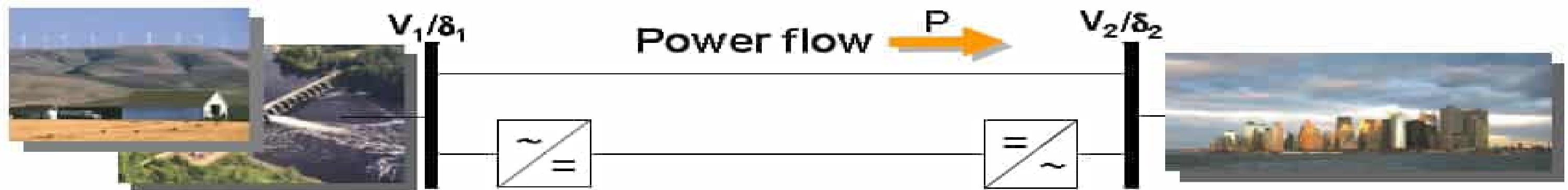
Sistemas de Alta Tension DC (HVDC)

PARAMETROS PRIMARIOS DE LINEA DE TRANSMISION

- ❖ Impedancia en Serie: ($Z=R+j\omega L$): Resistencia (R) & Inductancia (L)
- ❖ Admitancia en Paralelo: ($Y=G+j\omega C$): Conductancia (G) & Capacitancia (C)
- El perfil de voltaje de una linea de transmission depende principalmente de la distancia, el tipo de carga de la linea y la compensacion.
- Limites de Capacidad de Lineas:
 - a) *Limite termico: lineas cortas ($L < 50 \text{mi} \sim 80 \text{ km}$).*
 - b) *Regulacion de Voltage: ($\pm 5\%$ of Voltaje Nominal) media ($50 \text{mi} \leq L \leq 150 \text{mi} \sim 241 \text{ km}$).*
 - c) *Estabilidad & Angulo Oscilacion: Mas comun en lineas largas ($> 150 \text{mi} \sim 241 \text{ km}$).*
- El factor principal de inestabilidad se debe a la inability de mantener el balance de potencia reactiva, el control de tensiones y frecuencia.
- En un sistema interconectado estable, la demanda de potencia activa y reactiva tiene que mantenerse todo el tiempo para evitar colapso de voltaje.
- La demanda de potencia reactiva debe satisfacerse localmente para maximizar el flujo de potencia activa desde las plantas generadoras para asi minimizar perdidas y mantener una operacion eficiente del sistema.

Formas de aumentar el flujo de potencia de una línea de transmisión:

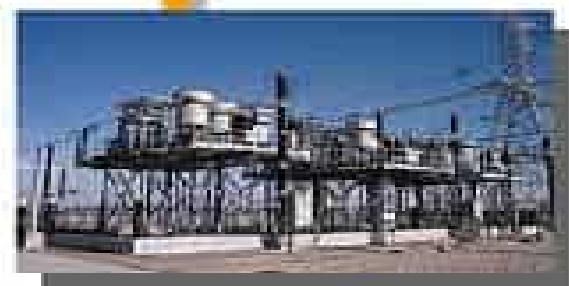
- Repotenciar la línea con conductores mas gruesos y/o mas conductivos
- Operacion dinamica de la linea monitoreando datos climaticos
- Agregar Compensador Estatico Reactivo (SVC o STATCOMS)
- Instalar Capacitores en serie y en paralelo (SCB)
- Emplear transformadores desfasadores (PST)
- Implementar Estacion Convertidoras AC to DC (HVDC)



$$P = \frac{V_1 V_2}{X_{12}} \sin(\delta_1 - \delta_2) + P_{HVDC}$$



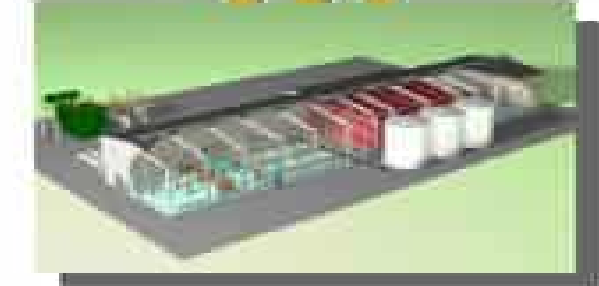
SVC & STATCOM
Boost or control ac
voltage (V), dynamic
reactive reserve



SC & TCSC – Boost
Voltage (V), Reduce line
reactance (X), limited by
voltage profile

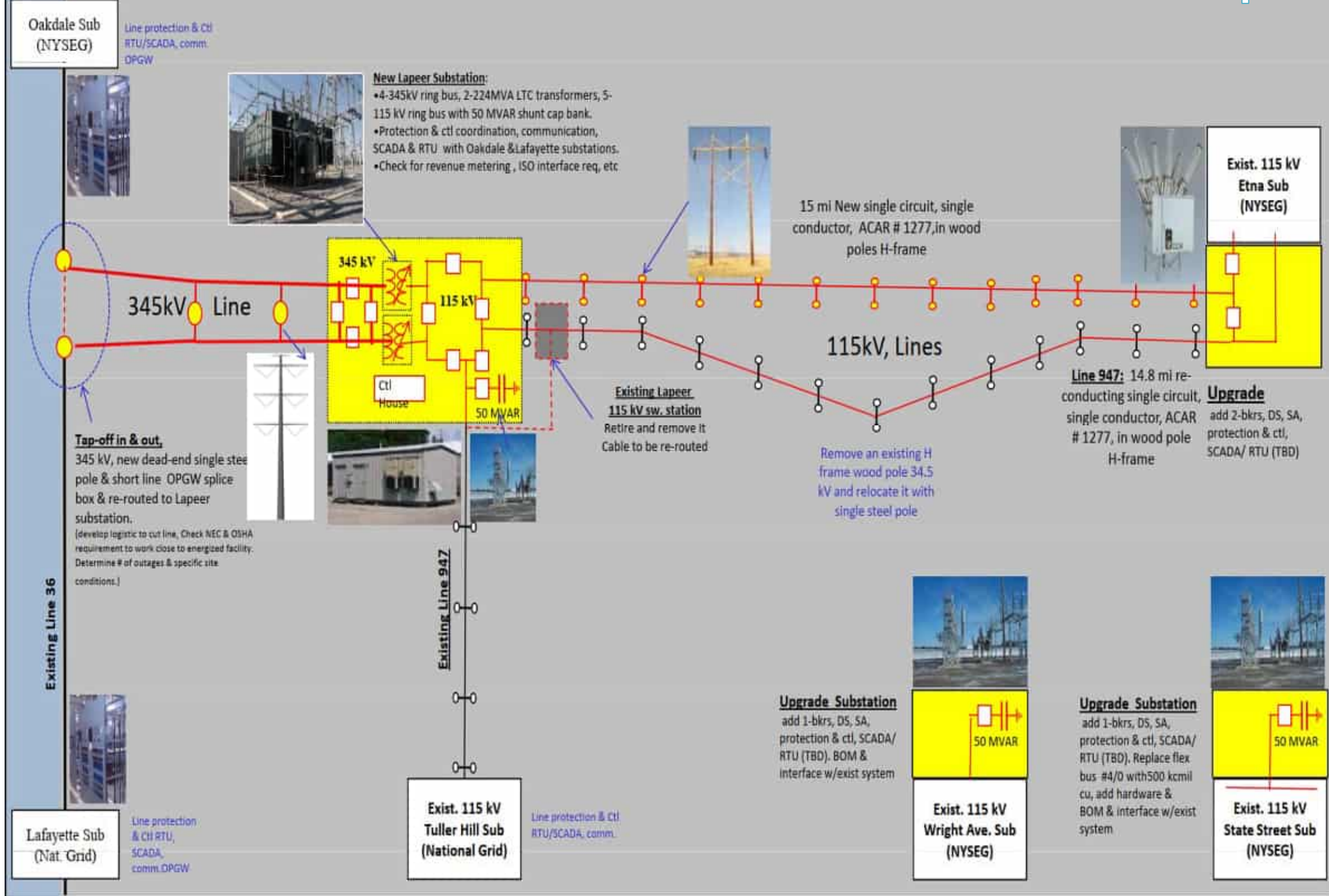


Phase Shifting Xfmrs -
Regulate phase angle (δ),
limited by MVA, angular
range



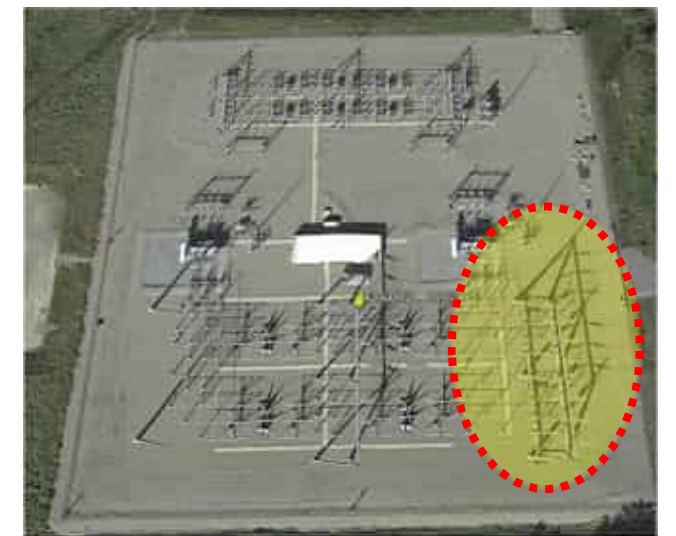
HVDC & HVDC Light -
Control power flow (P) and
ac voltage (V), leverage ac
cap by dynamic Q

60km Lineas 345/115 & 35kV- 2 Subs & 4 Shunt Cap.

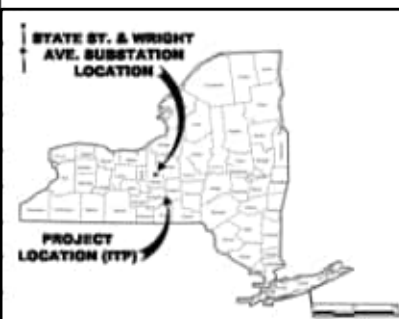
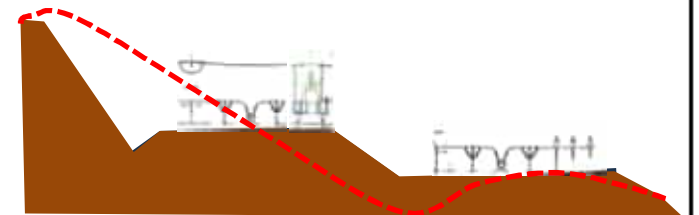


DESCRIPCION PROYECTO EPC

- **Substaciones:**
 - Substacion Clarks Corner Substation: 4-345kV en anillo, 2-224MVA transformadores con LTC and 5-115 kV con cap bank.
 - Modernizar 4 substaciones 115kV:
 - **Etna Sub (NYSEG)** - add 2-bkrs, DS, SA, protection & cti, SCADA/ RTU.
 - **Weight St (NYSEG)** - add 50 MVAR cap bank, bkr, SA, Prot. & cti, SCADA/ RTU.
 - **State St (NYSEG)** - add 50 MVAR cap bank, bkr, SA, replace conductors prot & cti, SCADA/ RTU.
 - **Tuller Hill Sub (National Grid)** - protection & cti, SCADA/ RTU.
- **Lineas de Transmision (PLS CAD, topografia)**
Cortar linea existente (in & out) a nueva subestacion.
- ✓ **Ingenieria Civil & permisos de Medio ambiente:**
- ✓ **Compra y Suministro de Equipos.**
- ✓ **Administracion de Construccion**
- ✓ **Pruebas y Puesta en Servicio.**



Clarks Corners Substation

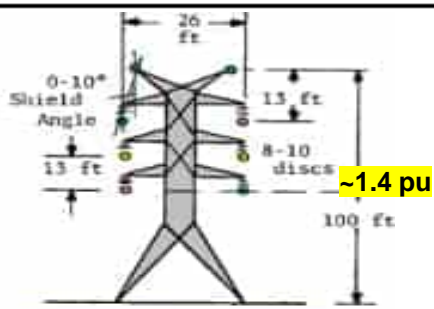


New York State
Electrical & Gas Corp.

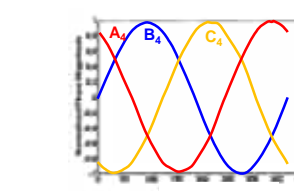
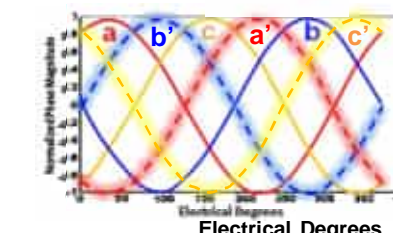
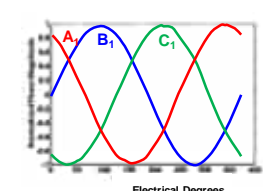
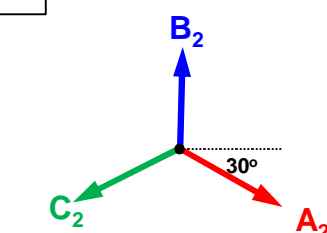
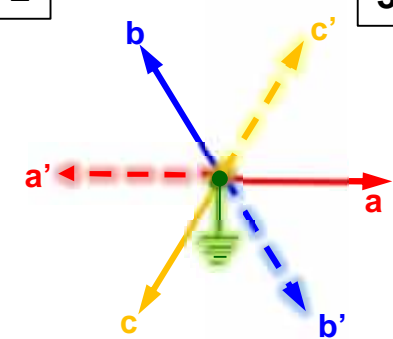
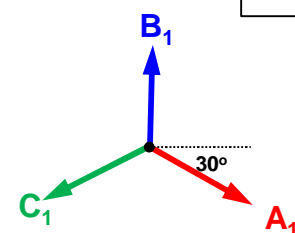
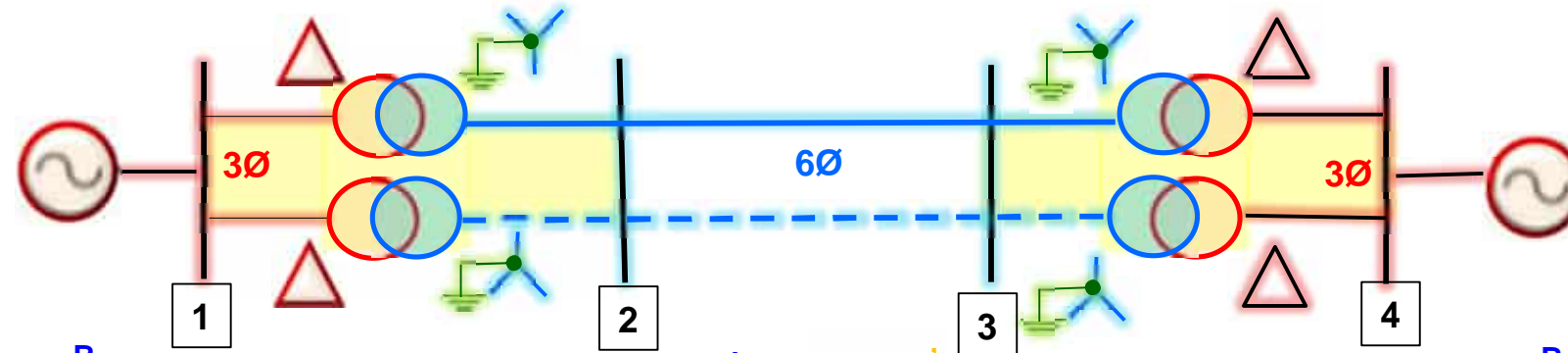
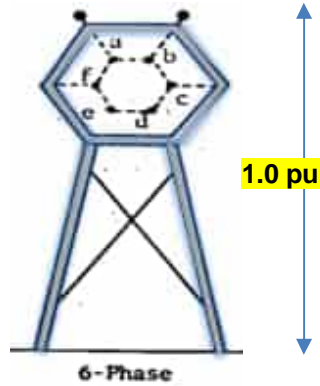
ALCANCE DEL PROYECTO
Sistema de Transmision Ithaca



Interconexion Hexafasica



Conventional
80 kV ϕ -G Double Circuit
80 kV Phase-to-Ground
138 kV Phase-to-Phase



Tension $\phi\phi$ Nominal (kV)	Capacity Linea (MW)	
	3 Phase	6 Phase
69	250	433
115	417	722
138	501	867
230	835	1444
345	1252	2167
500	1815	3140
750	2723	4710

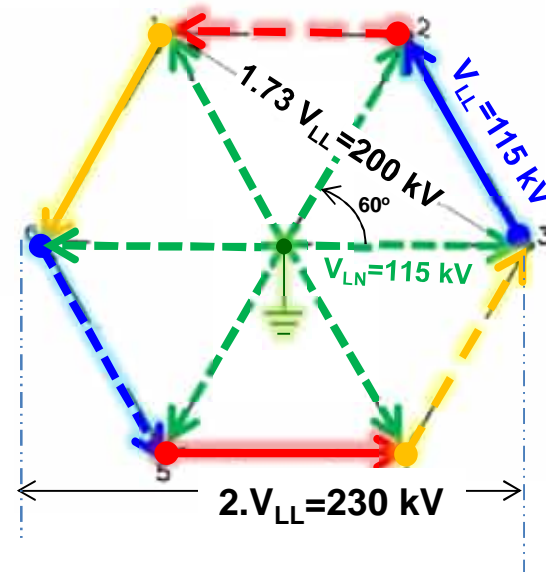
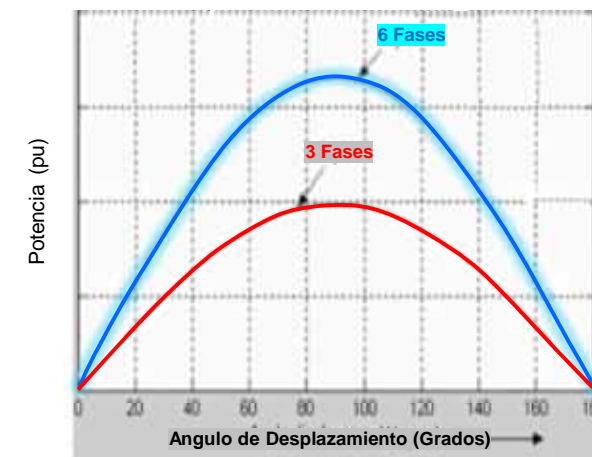


Diagrama Fasorial Hexafasico



Estabilidad Transitoria

- **Principio Basico:** Maximizar la densidad de potencial transmitida incrementando el voltaje de fase-tierra hasta el voltaje de fase-fase manteniendo las tensiones de fase-fase de conductores adyacentes sin alterar el calibre del mismo o los aisladores de linea.
- **Resultados:** Elevar la capacidad de Transmision de potencia hasta 73% y reducir costos.
- **Ventajas Adicionales:** Incrementar la capacidad termica de la linea, reducir la diferencia de angulo de fase entre voltajes transmisor y receptor y puede reducir la franja de servidumbre.
- **Desventajas:**
 - Experiencia reducida de operacion y mantenimiento.
 - Gradiente a tierra mas alto incrementa campo electrico a tierra.
 - Sistema de proteccion y control mas complejo.
 - Modelaje del Sistema mas dificil.





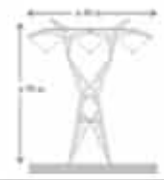

NYSEG New York State
Electrical & Gas Corp.

**DATOS TECNICOS PARA
CONVERSION DE 3 A 6 FACES**

EBASCO Electric Bond and Share
Company

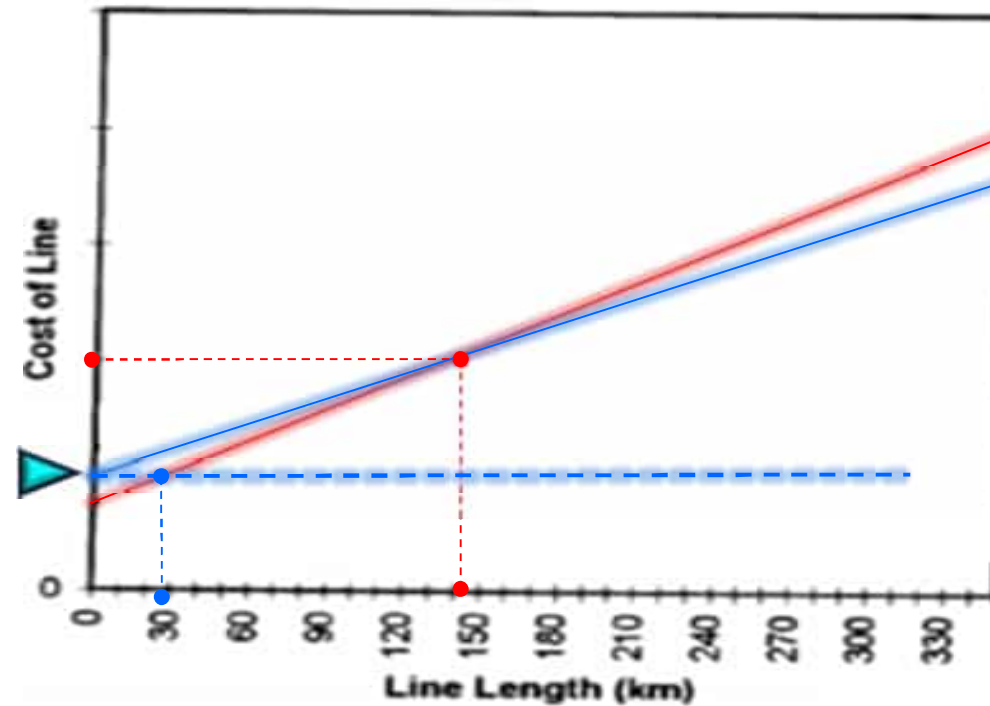
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SUMMARY DATA AVAILABLE FOR TWO HIGH PHASE ORDER PROJECTS

Item	Reference Project	Utility	Length (mi)	SIL (MW)	+ Sequence (pu)		Exist. 3φ Voltage		New 6φ Voltage		Total Cost / Cost Ratio (6φ/3φ)	Line Cost / Cost Ratio (6φ/3φ)	Breakeven Distance (mi)	Comments
					R	X	∅∅(kV)	∅n (kV)	∅∅(kV)	∅∅(kV)				
1.1	Goudey-Oakdale (Binghamton, NY-USA) 1992	NYSEG	1.5	72	0.090	0.289	115	66.4						There is a break-even distance, varying with the particular circumstances, at which six-phase line cost savings overcome higher terminal costs to make six-phase construction an attractive alternative for upgrading an existing double-circuit line. This break-even distance was 23-28 miles for an existing 115-kV double-circuit three-phase line.
1.2				119	0.046	0.174			93	93	\$10.9M	0\$	28	
1.3				243	0.023	0.085			133	133				
2.0	Camden -Duvha (Mozambique, S. Africa) 1998	ESKOM	62	636	N/A	N/A	400	230.9	173	173	\$531.9 M	\$283.5 M	140	The 6-phase line on the other hand, must have costly terminal equipment installed at both ends of the line for both voltage transformation, and phase shifting. Line feeder bays must be installed for the line side breakers. Currently ESKOM shading electricity for 12 hours every day.
											187.6%	80.8%		

SURGE IMPEDANCE AND SIL OF THREE-PHASE AND SIX-PHASE TRANSMISSION LINES

Case name	Surge impedance(Ω)	SIL (MW)
138 kV three-phase double circuit tower line	491.0	78.2
80 kV six-phase conventional tower line	491.0	78.2
80 kV six-phase compact tower line	413.1	93.0
138 kV six-phase conventional tower line	491.0	231.7



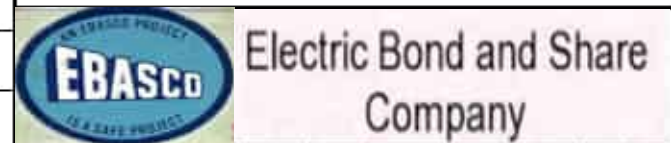
$$Z_{eq} = \begin{bmatrix} Y_{t_{1a1}} & Y_{t_{1a2}} & Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a2}} & Y_{t_{1a1}} & Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a2}} & Y_{t_{1a1}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a4}} & Y_{t_{1a3}} & Y_{t_{1a5}} & Y_{t_{1a6}} & Y_{t_{1a2}} & Y_{t_{1a1}} \\ Y_{t_{1a5}} & Y_{t_{1a6}} & Y_{t_{1a1}} & Y_{t_{1a2}} & Y_{t_{1a3}} & Y_{t_{1a4}} \\ Y_{t_{1a6}} & Y_{t_{1a5}} & Y_{t_{1a4}} & Y_{t_{1a3}} & Y_{t_{1a6}} & Y_{t_{1a5}} \end{bmatrix}$$

$$\begin{bmatrix} I_{1a1} \\ I_{1a2} \\ I_{1a3} \\ I_{1a4} \\ I_{1a5} \\ I_{1a6} \end{bmatrix} = \begin{bmatrix} Y_{t_{1a1}} & Y_{t_{1a2}} & Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a2}} & Y_{t_{1a1}} & Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a3}} & Y_{t_{1a4}} & Y_{t_{1a2}} & Y_{t_{1a1}} & Y_{t_{1a5}} & Y_{t_{1a6}} \\ Y_{t_{1a4}} & Y_{t_{1a3}} & Y_{t_{1a5}} & Y_{t_{1a6}} & Y_{t_{1a2}} & Y_{t_{1a1}} \\ Y_{t_{1a5}} & Y_{t_{1a6}} & Y_{t_{1a1}} & Y_{t_{1a2}} & Y_{t_{1a3}} & Y_{t_{1a4}} \\ Y_{t_{1a6}} & Y_{t_{1a5}} & Y_{t_{1a4}} & Y_{t_{1a3}} & Y_{t_{1a6}} & Y_{t_{1a5}} \end{bmatrix} \begin{bmatrix} E_{1a1} \\ E_{1a2} \\ E_{1a3} \\ E_{1a4} \\ E_{1a5} \\ E_{1a6} \end{bmatrix}$$



REVISION APPROVAL RECORD				REV		REV		DATE		REVISIONS		BY	CHKR	DRAWING STATUS				Aditado para Presentacion		
DISCIPLINE	BY	DATE	DISCIPLINE	BY	DATE									ISSUED	REV	DATE	SDE	PEM	DRN:	DATE:
ARCH.			MECHANICAL											PRELIMINARY	A	04-25-24		AP		
CIVIL			NUCLEAR																CHKD:	DATE:
ELECTRICAL			PIPING																	
ENVIRON.			PROCESS											APPROVED FOR CONSTRUCTION						
GEN. ARRANG.			QA / QC																	
HVAC			STRUCTURAL																	
I & C																			SCALE:	NTS

DATOS ECONOMICO INDICATIVO CONVERSION DE 3 A 6 FACES



Interconexión con Superconductor de Alta Temperatura NYC – US\$40M

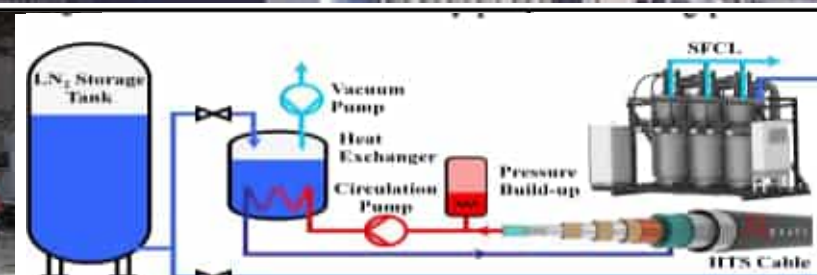
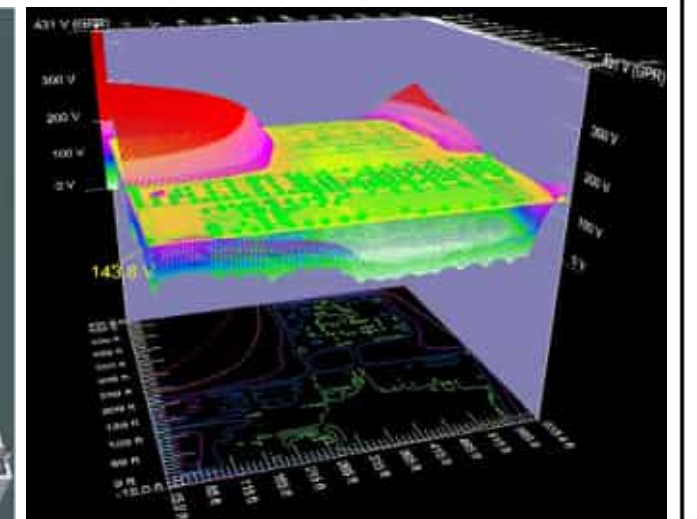
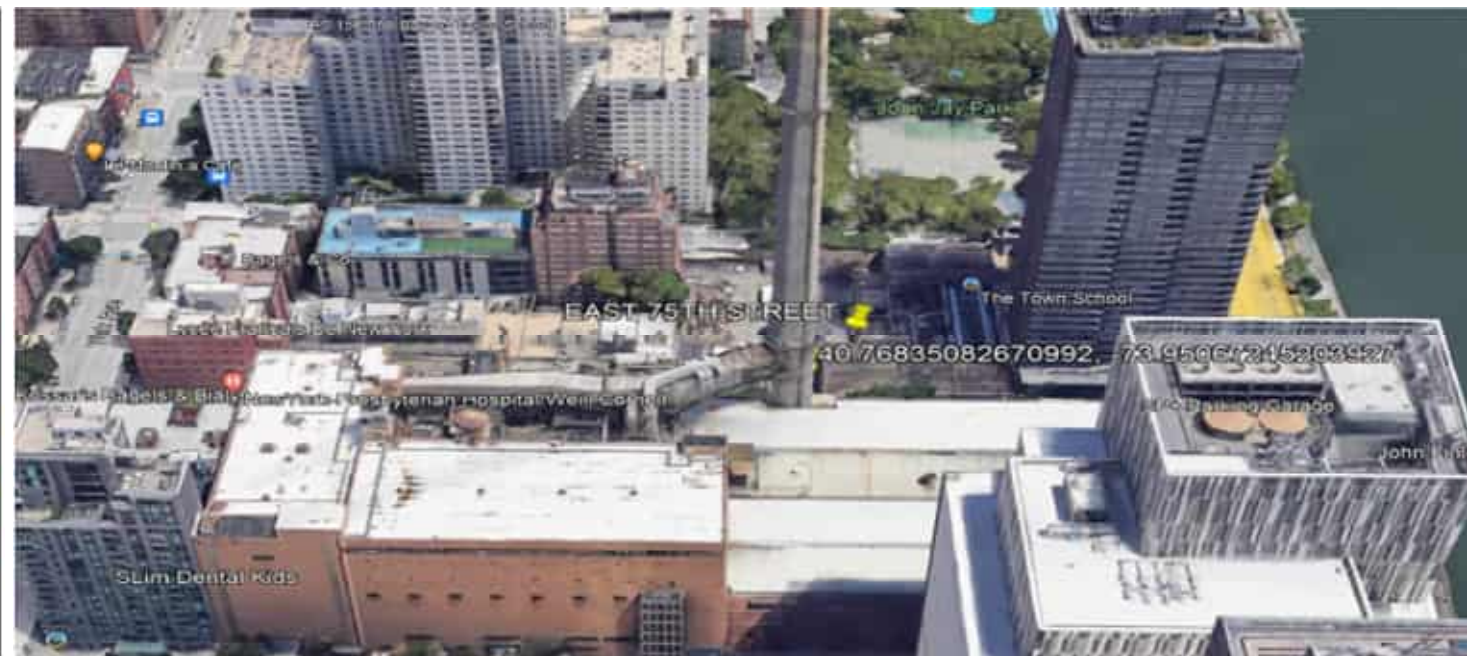
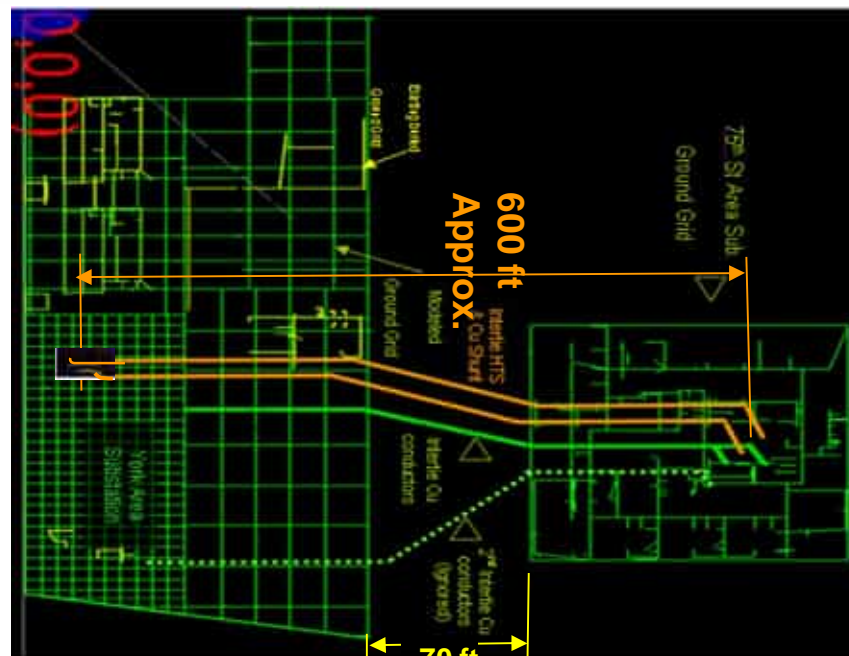
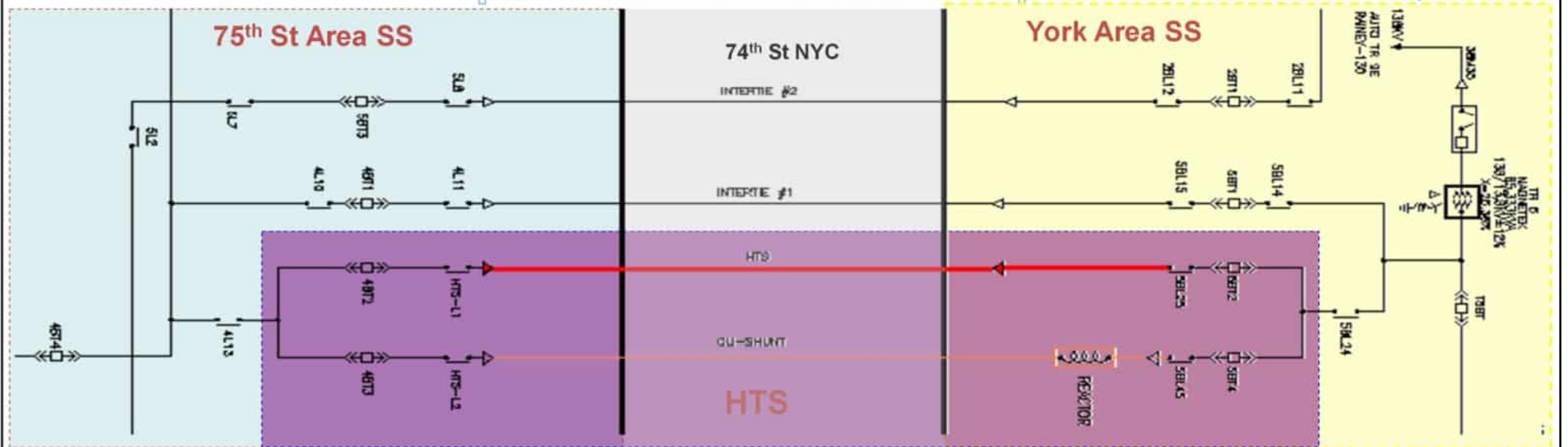
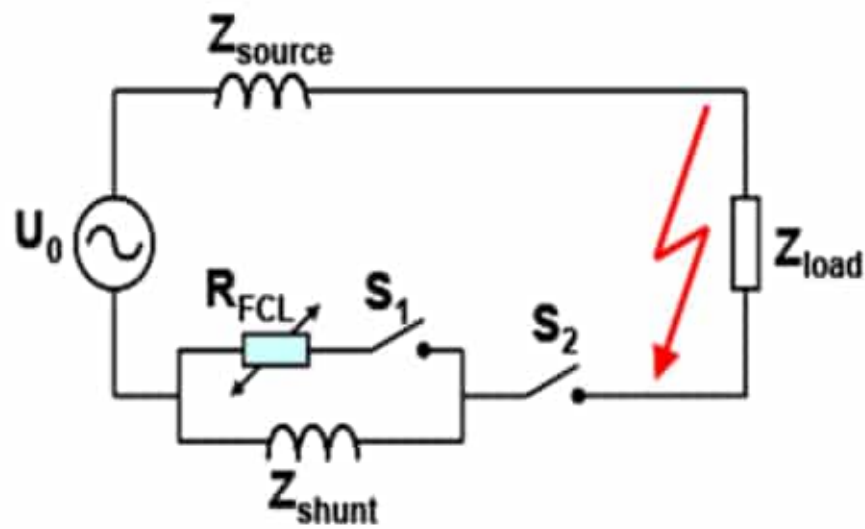


Figure 4 Schematic of cooling system for AmpaCity

conEdison
Consolidate Edison
Of New York State

Superconductor y Aplicación en
Reducción de Corriente Corto Circ.

URS



Scheme of a shunted limiter configuration.

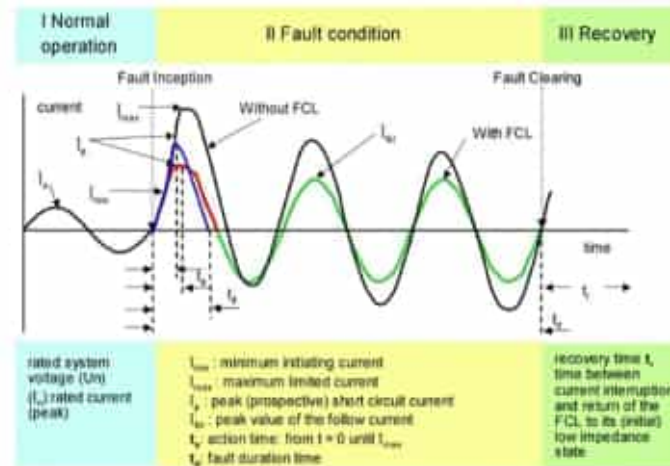
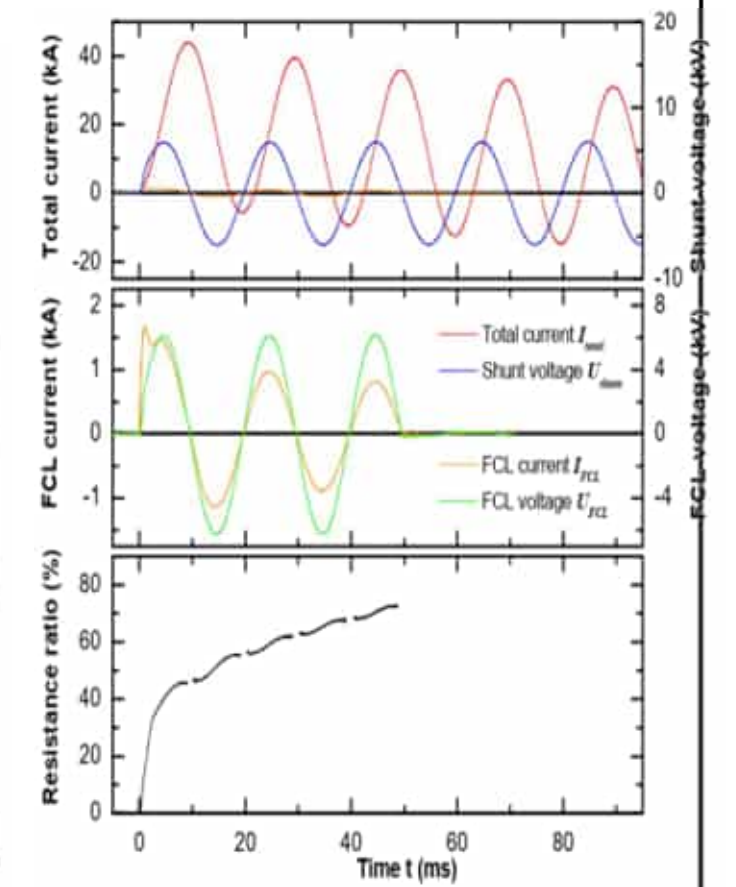
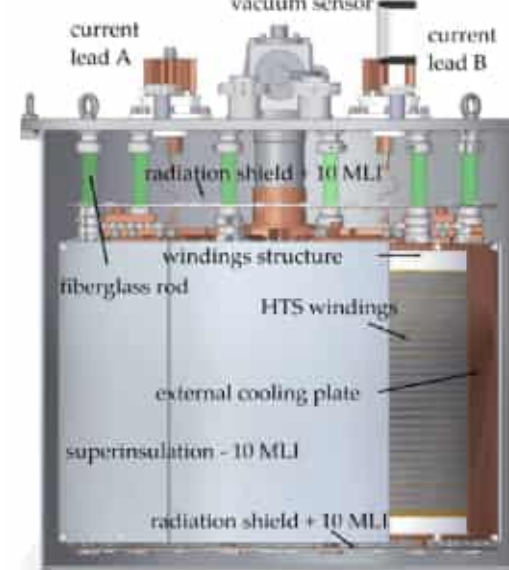
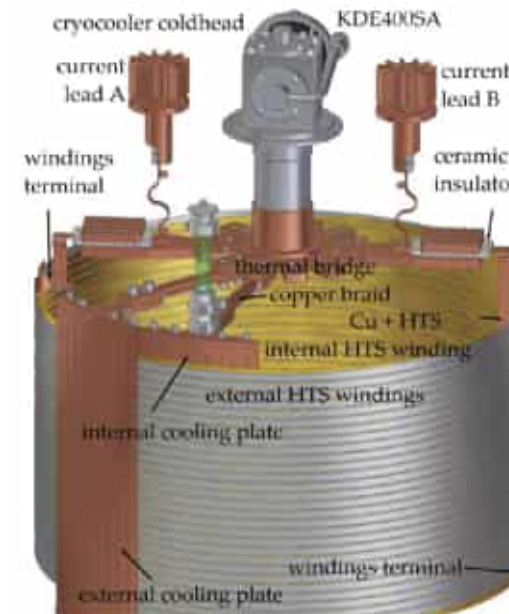
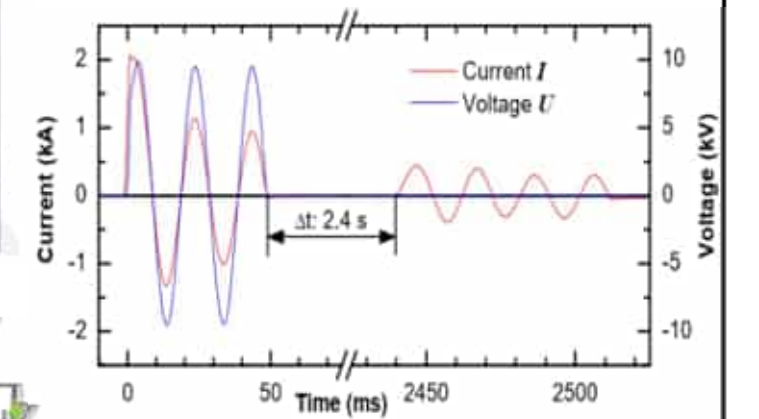


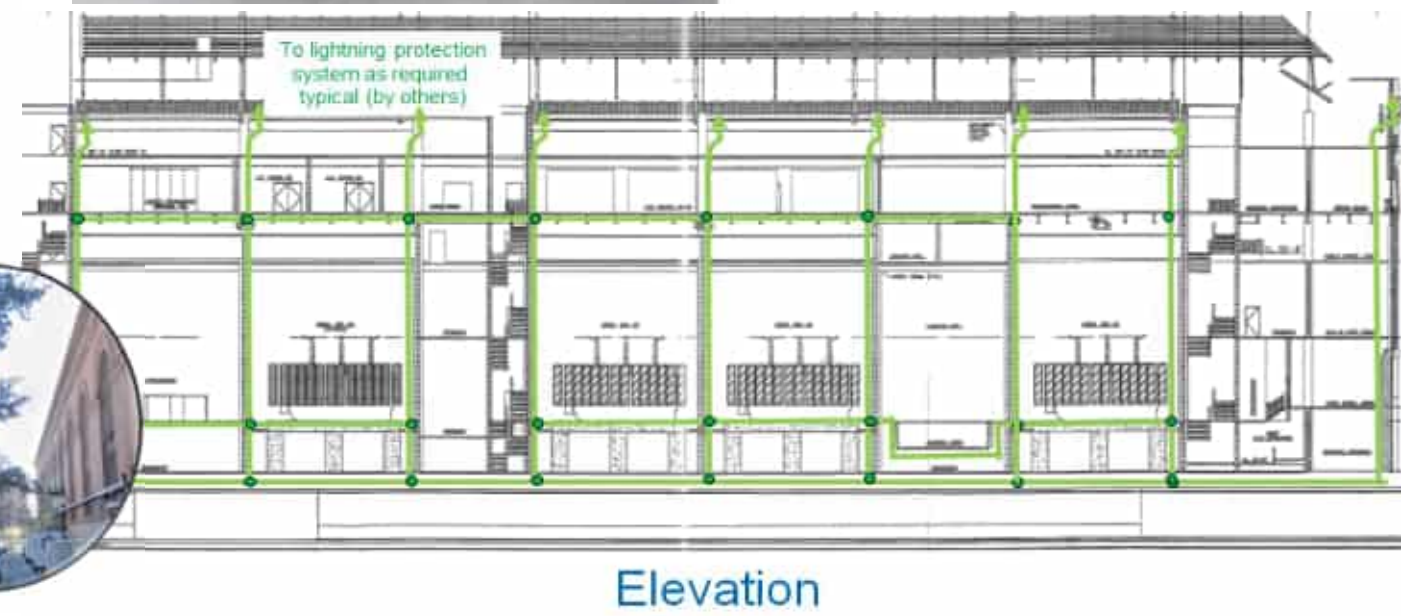
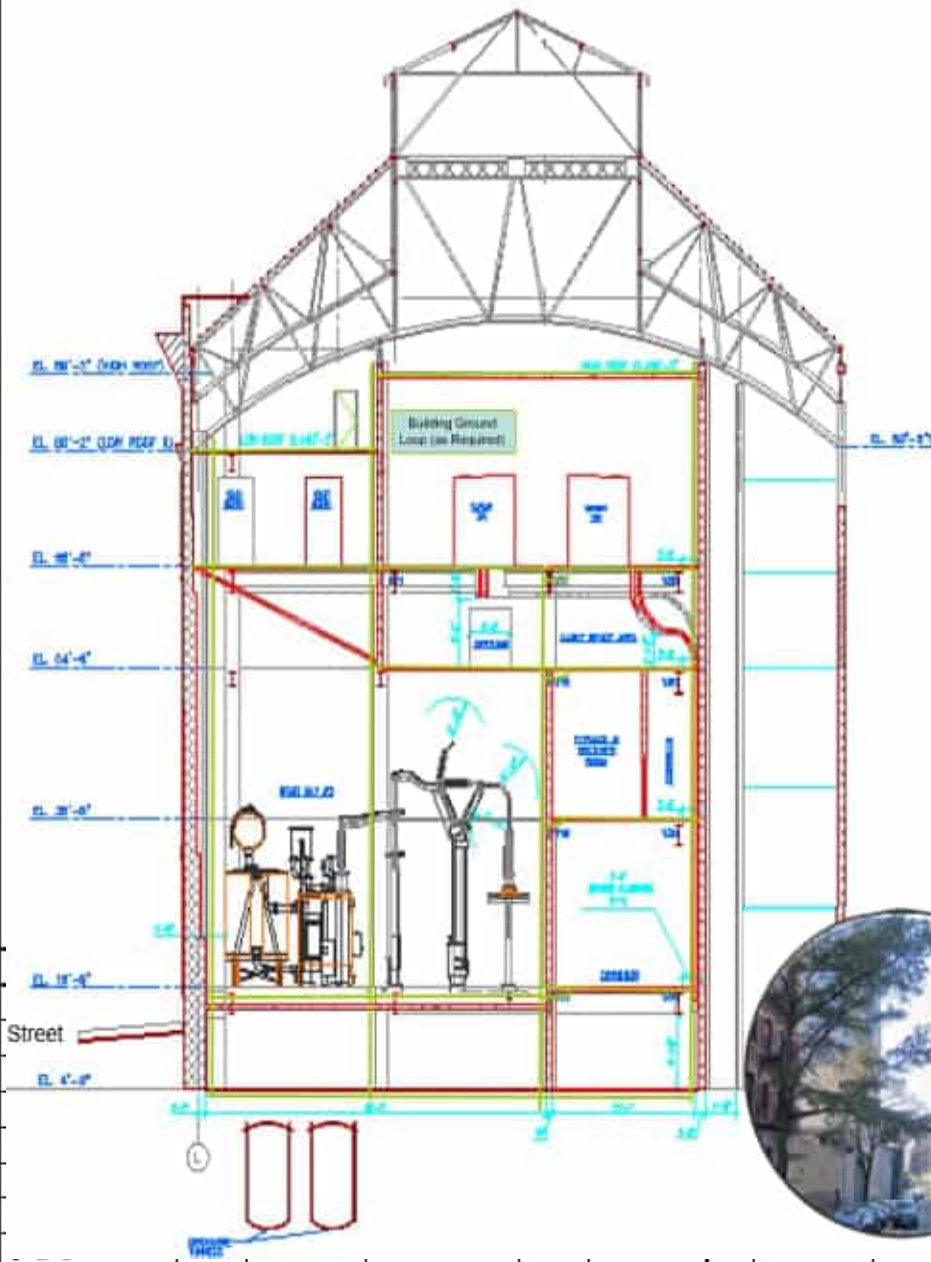
Fig 4.2 operation sequence of SFCL



Power test in shunted configuration, $U_0: 8.3 \text{ kV}$, $I_{\text{prosp}}: 34 \text{ kA}_{\text{rms}}$, $\phi_{\text{start}} = 0^\circ$.



Demonstration of recovery time.



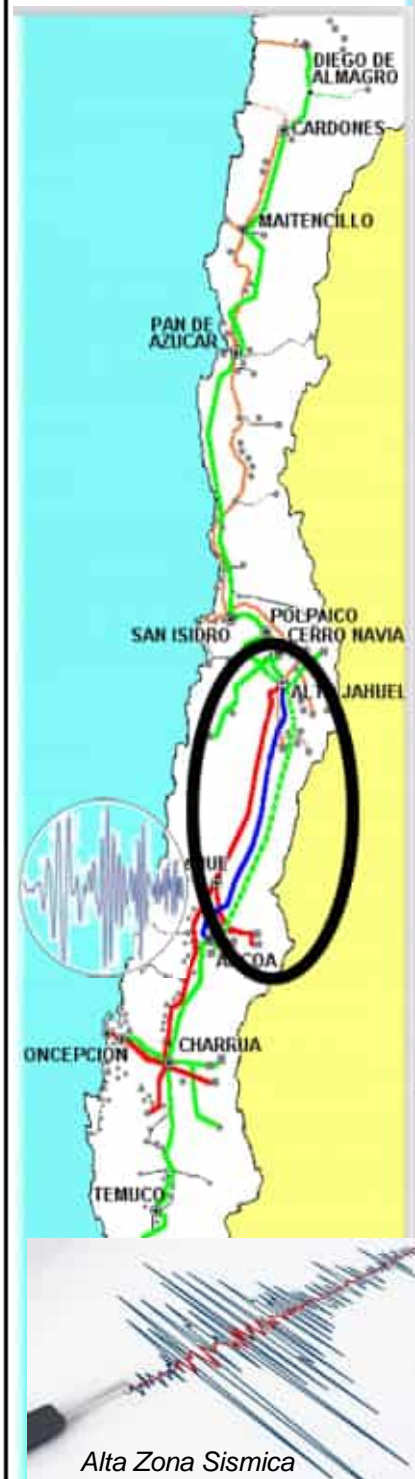

 Consolidate Edison
 Of New York State

Supperconductor y Aplicacion en Reduccion de Corriente Corto Circ.

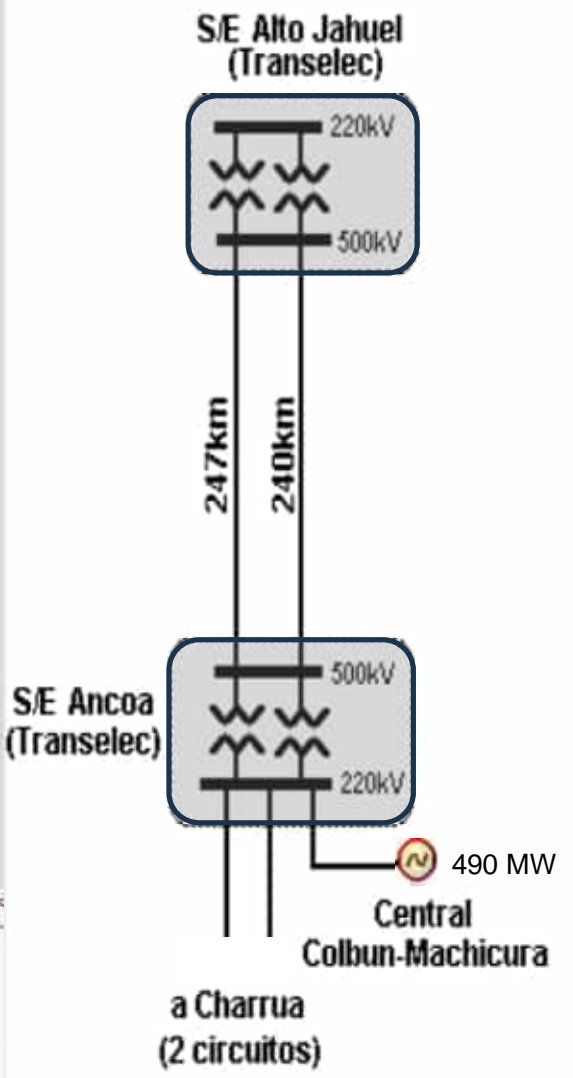


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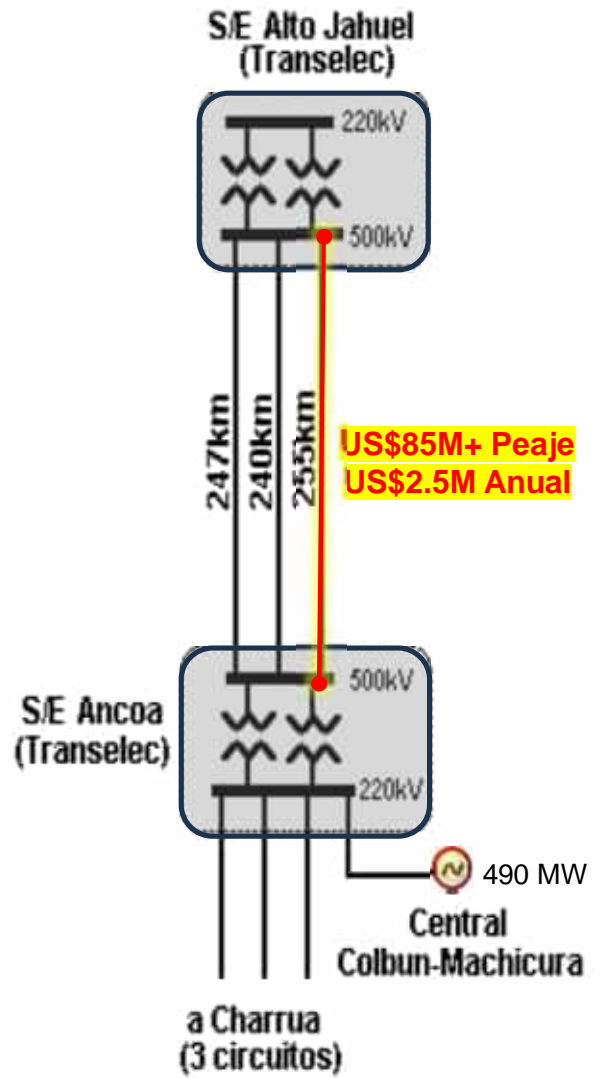
255 km Linea con Compensacion Capacitiva Serie ~US\$75M Colbun Chile



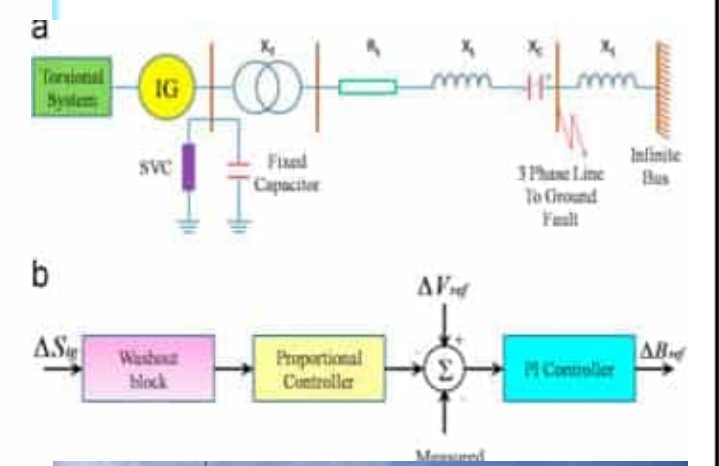
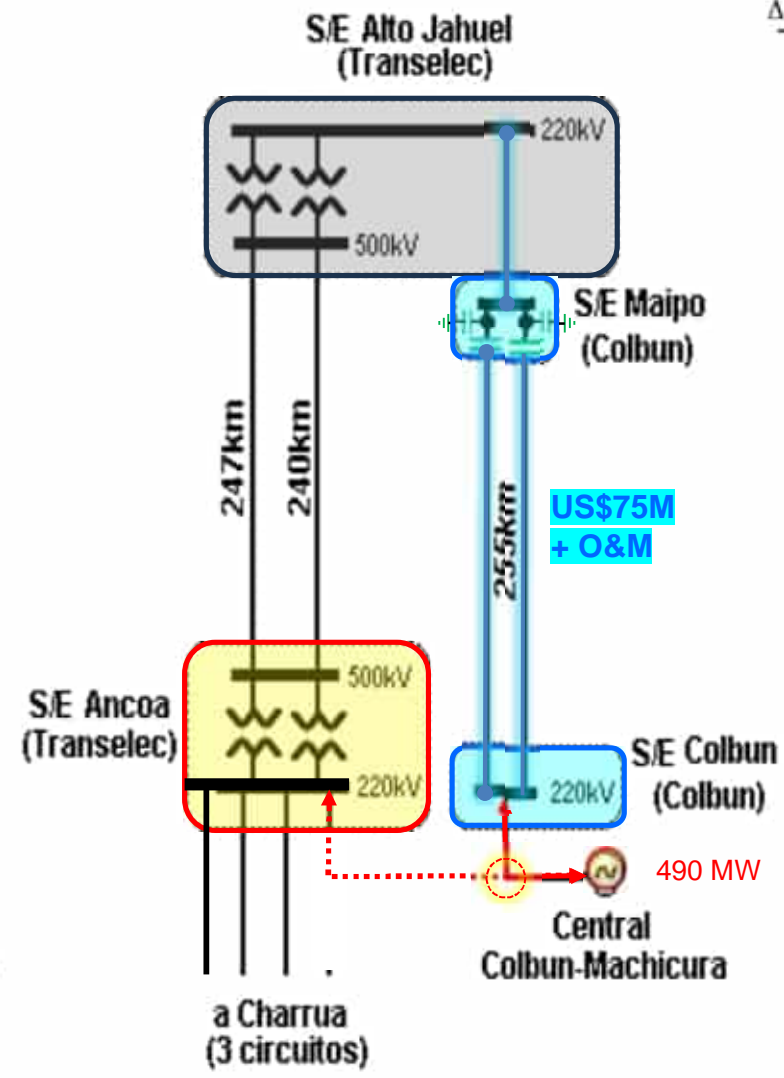
1996 system



Transelec expansion proposal



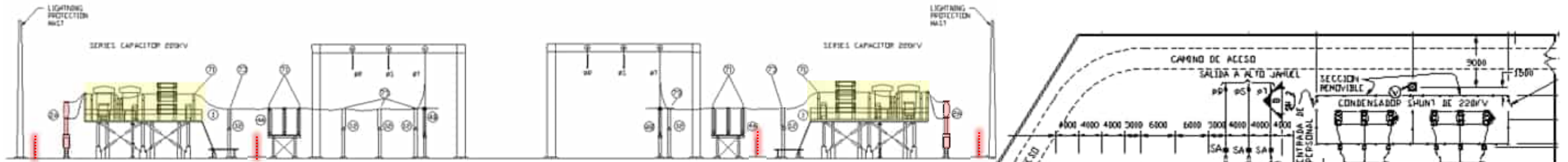
Colbun solution 1997



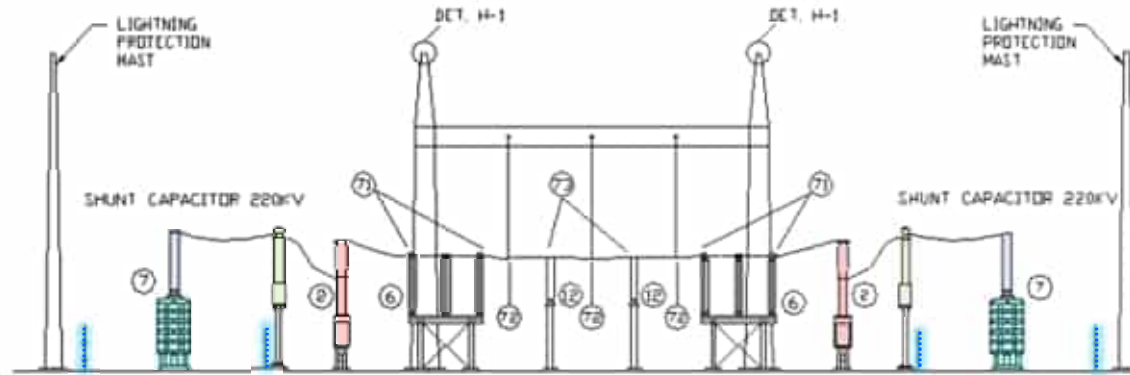
Superconductor y Aplicacion de Reduccion de Corriente Corto Circ.



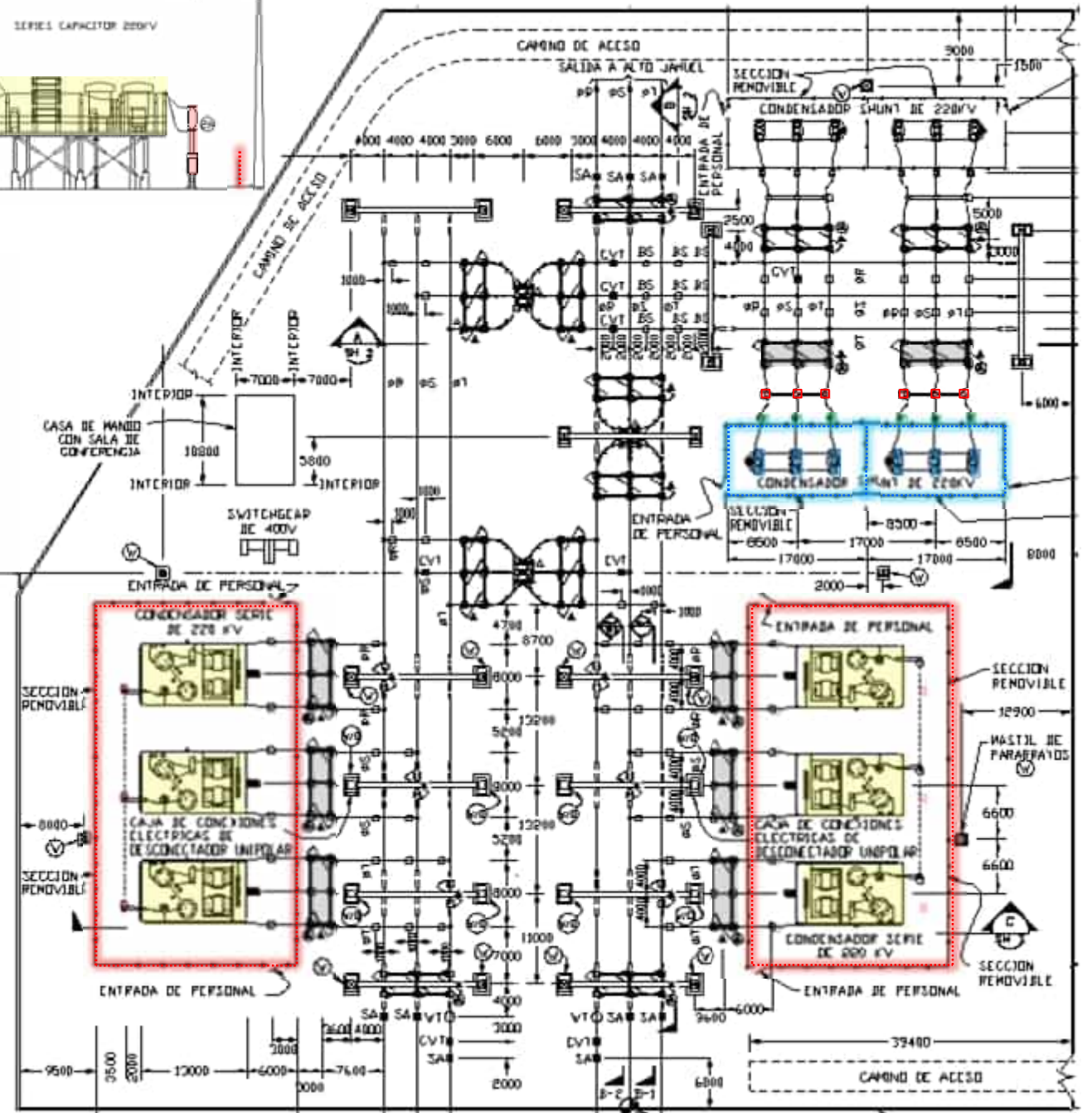
300 km Linea con Compensacion Capacitiva ~US\$75M Colbun Chile



Seccion Condensadores Serie



Seccion Condensadores Shunt



REFERENCIAS

Empresas coordinadas del COEC-SEC

LINEAS - KV

- 500
- 220
- 134
- 110
- 60 o menores

CENTRALES HIDROELECTRICAS

CENTRALES TERMoeLECTRICAS

SUBESTACION

NUDO



SDE		PEM		Aditado para Presentacion	
			AP	DRN:	DATE:
				CHKD:	DATE:
STRUCTION UNLESS SIGNED PRINTS BEARING EARLIER				SCALE:	NTS



580 km Linea, 2 Plantas & SVC~US\$500M - Electroandina Chile

Interconexión SING-SIC en la perspectiva del tiempo.

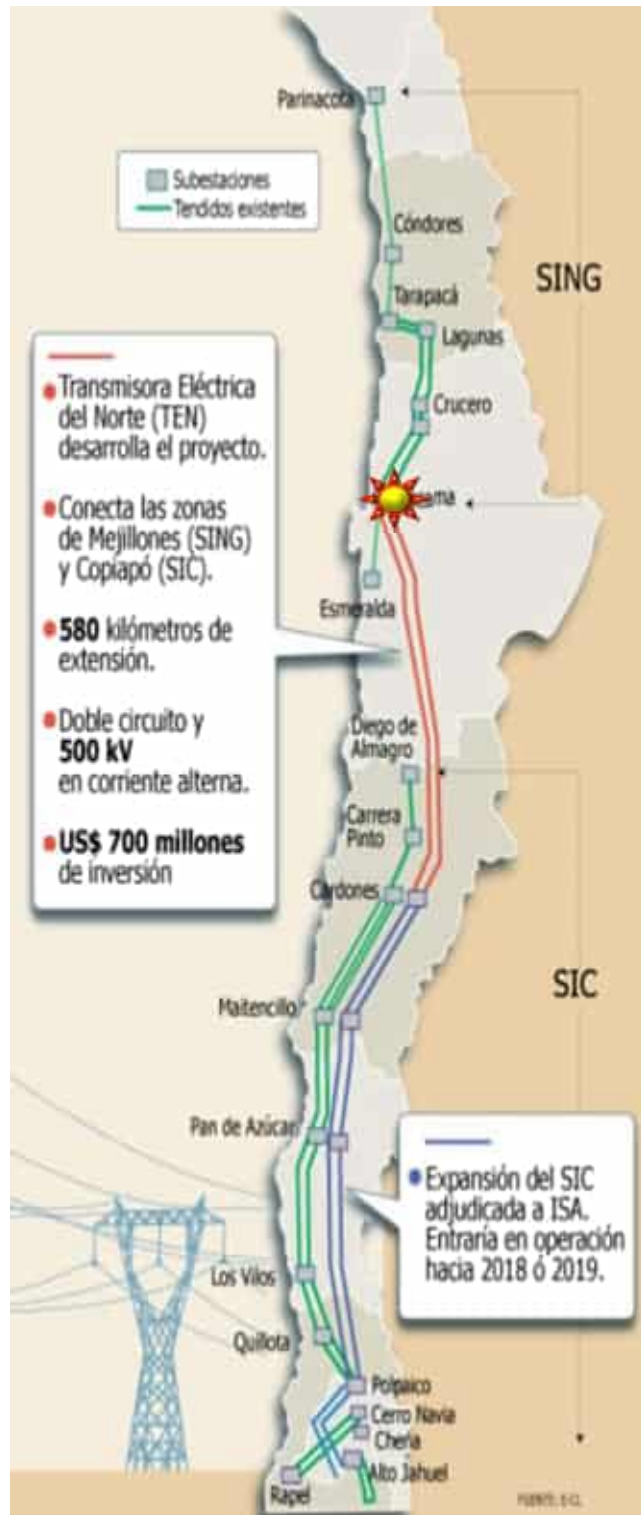
Texto Junio 2015: Edzard Zapata Helmig, periodista.

"En una conversación sostenida con Elio Cuneo respecto de como expandir el mercado objetivo de la empresa más allá del SING, dado que vislumbrábamos que los niveles de demanda de energía tenían límites, que el nivel de competencia que se esperaba en el futuro en el SING era muy duro y como las oportunidades que existían en la zona norte del SIC se veían atractivas, surge la idea de impulsar un proyecto de transmisión para la interconexión entre los sistemas SING y SIC, que permitiera llegar de manera competitiva al promisorio mercado del norte del SIC".

Por esto último, se exponen los conceptos asociados a Jos Remacle, Gerente General de la época, quien da el visto bueno para definir el trazado para el proyecto de transmisión entre Mejillones y Diego de Almagro.

En octubre de 1997, el presidente del Directorio de Electroandina S.A., Yves Jourdain, da a conocer la implementación de un plan estratégico que establecía la interconexión del SING y el SIC en 220 kV y la construcción de unidades a ciclos combinados que consideran gas natural importado de Argentina como insumo principal.

- El Sistema Interconectado del Norte Grande (SING) se extiende entre Tarapacá y Antofagasta,
- El abastecimiento eléctrico de los distintos centros de consumo se inició con sistemas locales independientes entre sí y destinados exclusivamente a resolver sus necesidades.
- Escasos recursos de agua para usos de generación eléctrica con un clima de extrema sequedad.
- Centros de consumo de electricidad separados por grandes distancias. Consumo de energía corresponde principalmente a empresas mineras.
- A fines de 1987 se interconectaron algunos de estos sistemas, dando origen al Sistema Interconectado del Norte Grande.
- El 30 de julio de 1993 comenzó la operación coordinada de las instalaciones del SING al constituirse el Centro de Despacho Económico de Carga (CDEC) del SING



Elio Cuneo H.



Luis Hornazabal,
Gerente Comercial y Desarrollo de la época.

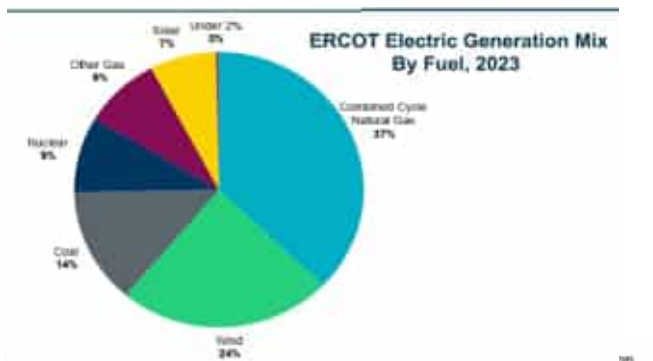
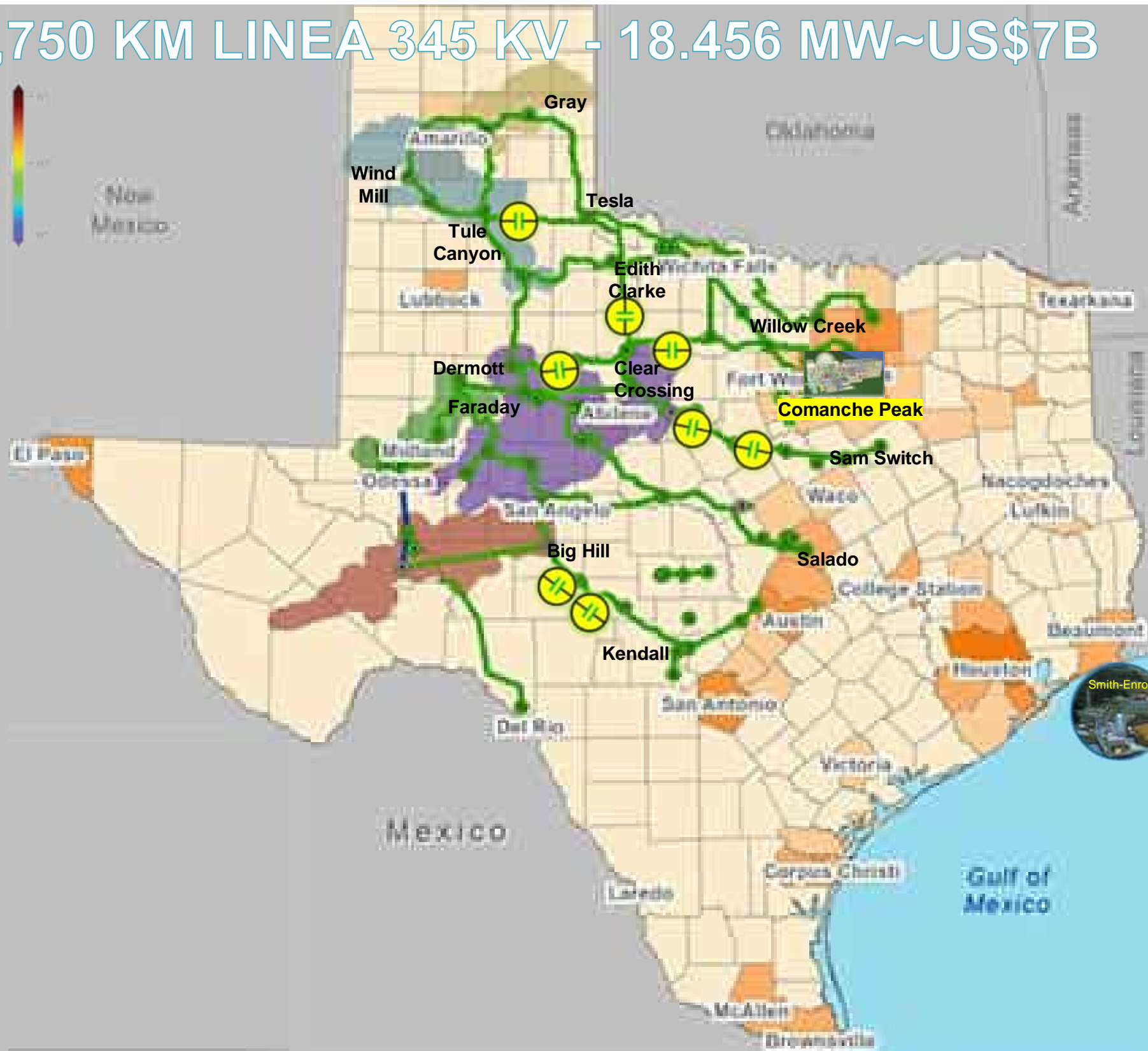
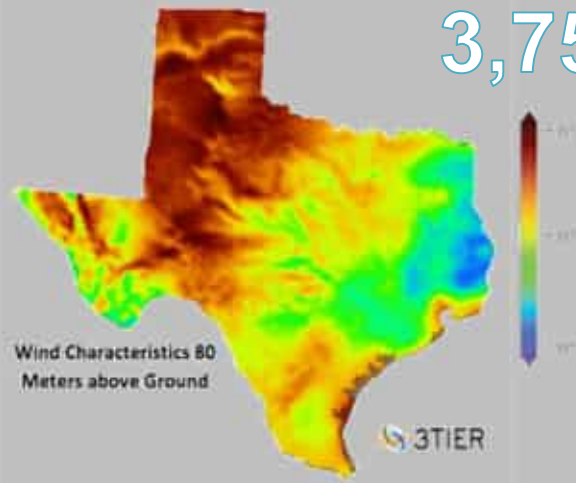
ABB wins US\$ 310-million order for Chile power plants

Press release | Zurich, Switzerland | 1998-07-29

Two 400-megawatt power plants for Chile's deregulated electricity market



3,750 KM LINEA 345 KV - 18.456 MW~US\$7B

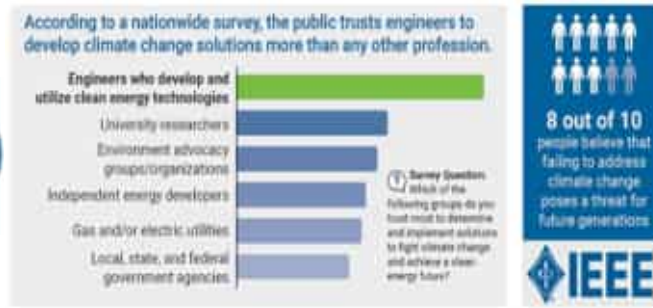


Optimization Study Options

	Option 1 (PTW)	Option 2 (PTW)	Option 3 (PTW)	Option 4 (PTW)
Zone 3A	1,453	3,191	4,960	4,480
Zone 4	1,047	2,293	3,730	
Zones 5/6	829	1,859	2,890	4,190
Zone 9A	1,208	3,047	4,770	3,610
Zone 19	419	1,063	1,631	1,081
CREZ transfer capability	9,700	11,553	17,954	17,514
Total transfer capability	13,715	18,456	24,019	24,415

Source: ERCOT (2008); Leber (2008)

	TOTAL REQUIREMENT		
	Min Export	Initial Build	Max Export/Edison
Series Capacitor	50% - 12 Lines	50% - 12 Lines	50% - 12 Lines
Shunt Reactors	3930 MVARs	3930 MVARs	3930 MVARs
Shunt Capacitors	0	660 MVARs	1136 MVARs
SVCs or STATCOMs	0	1400 MVARs	5300 MVARs
Synchronous Condensers	0	0	700 MVA



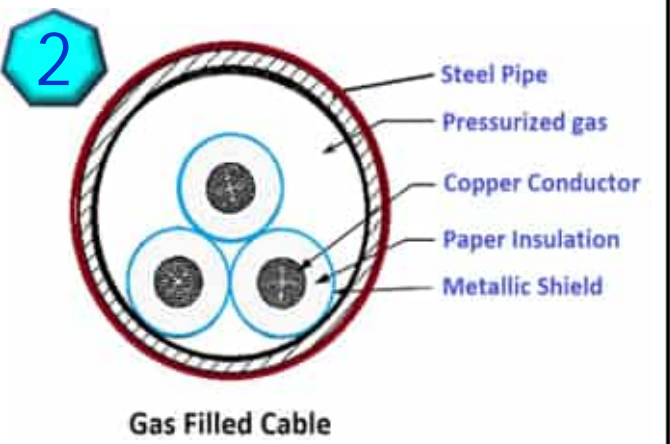
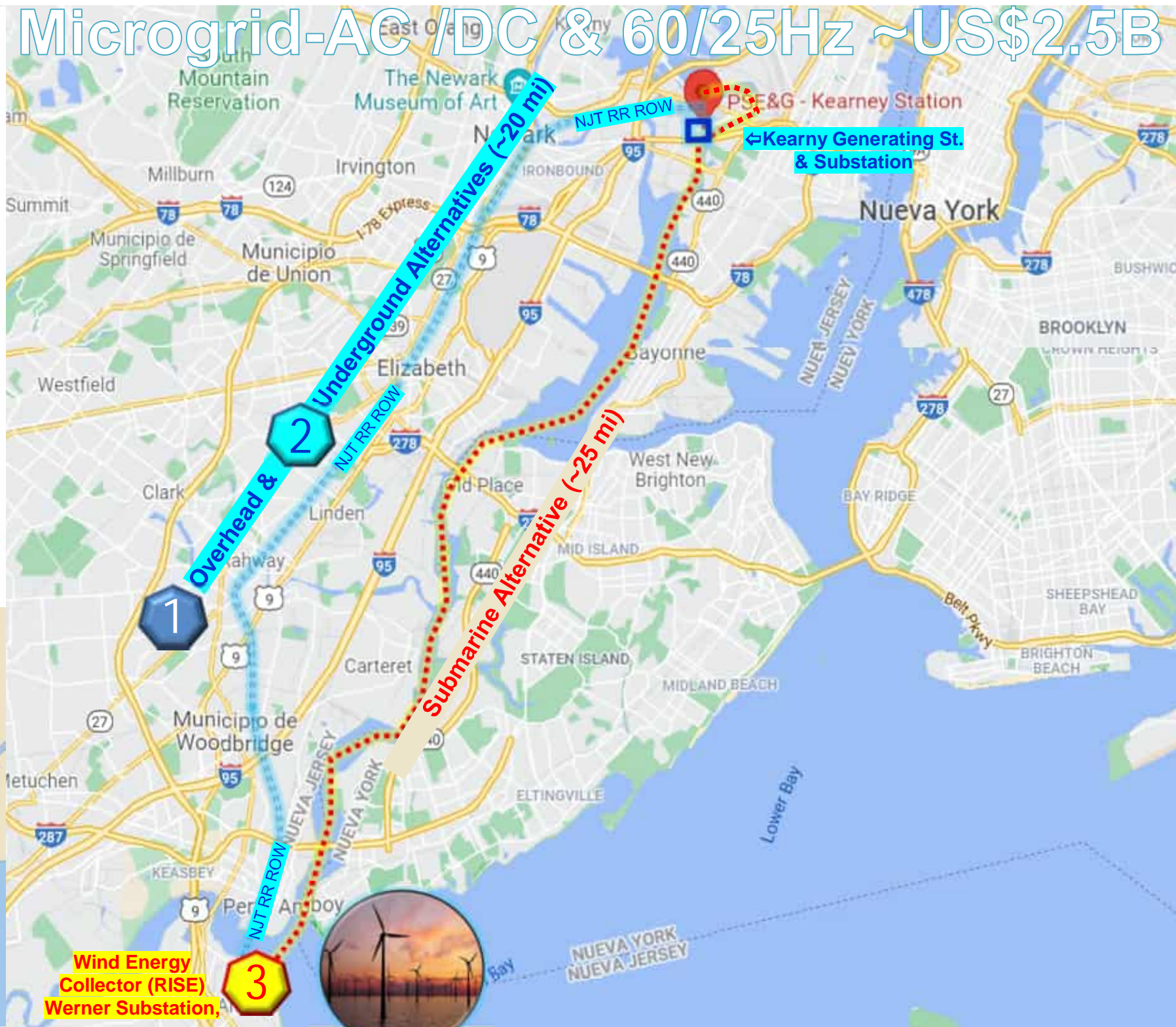
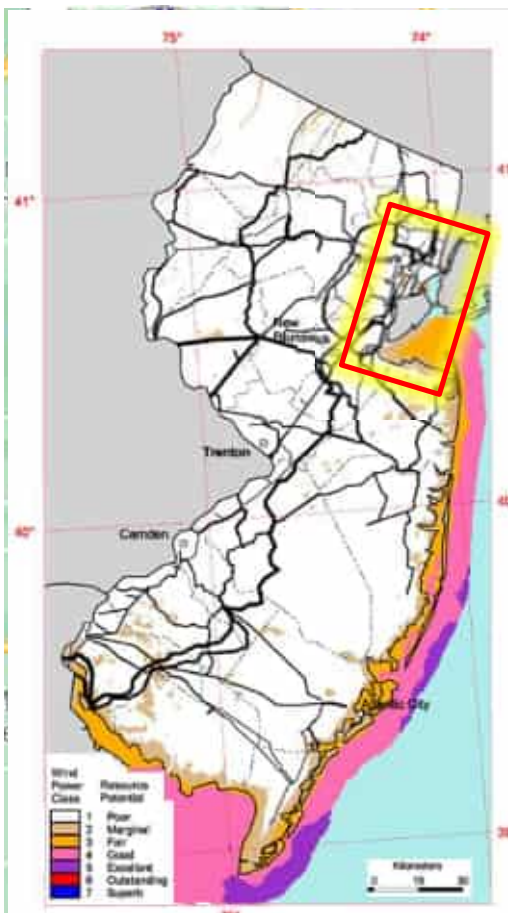
- ETT Project Summary
- 422.5 mi 345 kV lines
 - 7 new subs. 345 kV
 - 8 HV series capacitors
 - 7x2 shunt reactors
 - 3 Static Vars Comp.



Competitive Renewable Energy Zone (CREZ)



Microgrid-AC /DC & 60/25Hz ~US\$2.5B

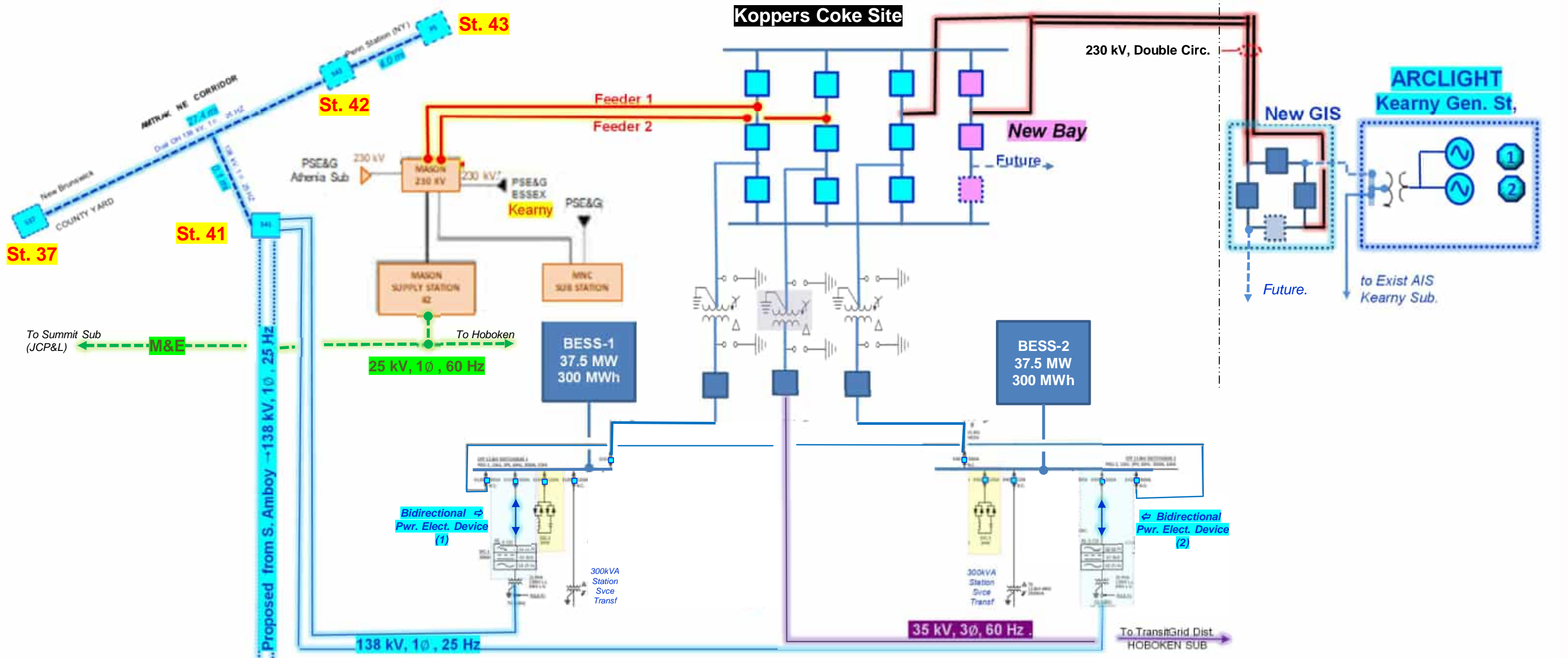


Item	Description	Distance Approx (mi)	Cost Reference			Challenger			Remark
			Cost Factor	Cost/mi (\$M)	Total Cost (\$M)	Permitting	Obstacles	Clearances	
1	Overhead Transmission line in the NJT RR corridor	20	1 (Base)	2.0	40	Red	Red	Red	Limited ROW, clearance constrains, crossing river and major highway, visible unpleasant. Wetland may require ACOE license and permit (L&P)
2	Underground line in the NJT RR corridor	20	8	16	320	Yellow	Green	Green	Acceptable ROW on NJT RR corridor, crossing other RR tracks, bridges & major infrastructures such as pipeline, gas, sewer & major highway. Water crossing and other obstacle require HDD and Jack & bore, ACOE L&P.
3	Submarin & UG Raritan Bay and Hackensack River.	25	10	20	500	Yellow	Green	Green	Submarine operation require spetial marine contractor (ex Codwell) and studies. Navigable water require ACOE L&P. Crossing under bridges and existing cables. Work compatible with cable installed by wind developer.

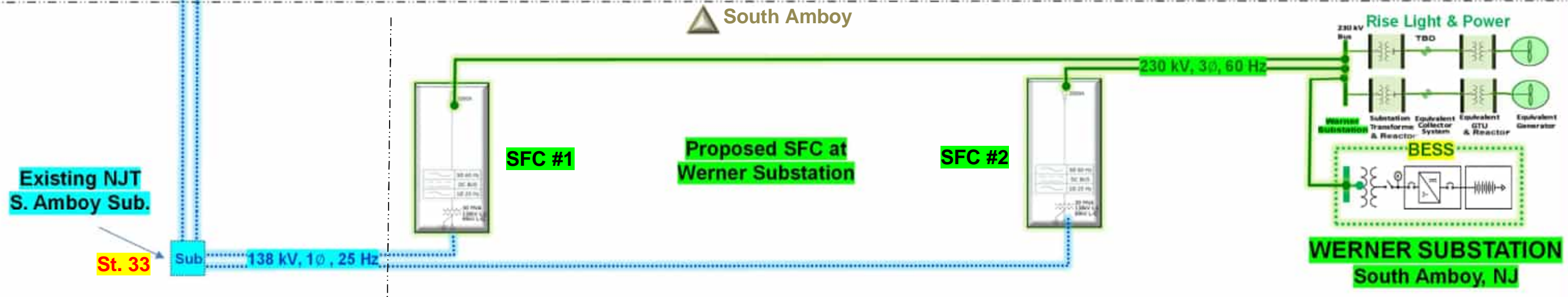
TRANSIT TRANSGRID MICROGRID PROJECT-RFP No 20-055

Alternatives for 230 kV Btwn. Werner & Mason Substations





South Amboy



← Select a location highlighted in blue to enter Street View.




**TRANSGRID MICROGRID
PROJECT-RFP No 20-055**

REVISION APPROVAL RECORD				REV	REV	DATE	REVISIONS				BY	CHKR	DRAWING STATUS				
DISCIPLINE	BY	DATE	DISCIPLINE	BY	DATE								ISSUED	REV	DATE	SDE	PEM
ARCH.			MECHANICAL										PRELIMINARY	A	04-25-24		AP
CIVIL			NUCLEAR														
ELECTRICAL			PIPING														
ENVIRON.			PROCESS										APPROVED FOR CONSTRUCTION				
GEN. ARRANG.			QA / QC														
HVAC			STRUCTURAL														
I & C																	

Aditado para Presentacion

DRN: DATE:

CHKD: DATE:

SCALE: NTS



UNITED
Engineers & Constructors



item	EQUIPMENT DECK	Qty
1	GIS Modules:	
	220kV (1 x B105 GIS, local cont, panel & marshalling box)	1
	69 kV (2 x T35 GIS, local cont, panel & marshalling box)	2
	Main transformer:	
	Rating: 280MVA; 230/69/69kV	1
2	Heat Exchanger (cooler)	2
1	Reactor 60MVAR, 230kV	1
5	Auxiliary transformers: (69kV/100V)	7
11	P&C Control Room (SCADA, Comm. & revenue metering)	7
13	AC & DC Auxiliary Power:	
	AC & DC load panels	4
14	Battery /UPS room	2
15	Diesel Gen Package (Noise enclosure, ATS & fuel tank)	1
	Ancillaries:	
	Fire protection & suppression system	1
	Heating, Ventilation and Cooling system (HVAC)	1
	Lighting system (illumination & navigation)	1
	Utility receptacle	1
	Lightning protection	1
	Public Address System (PA)	1
	Internal TV system (ITV) / CCTV	1
	Distribute Temperature Sensing (DTS)	1
	Interface Task:	
	GE Equipment & Design Data	1
	Platform Manufacturer	1
	Submarine Cable (Interconnection & attachment)	1
	Receiving end Utility (Comm., Rev. metering, ISO)	1

Notes:

- Wind farms are assumed to be installed in the sequence N3, N4, N2 and N1.
- Each of the N1 through N4 are assumed to consist of two wind farms each connected to a single ESP rated 250 MW for at total of 500 MW at each N1 through N4.
- A 230 kV AC tie is provided between each of N3 and N4, and between N2 and N1 for cable failure backup (the backup is limited to 500 MW).

Atlantic Wind Connection (AWC)
230kV/69kV Substation
Offshore Platform

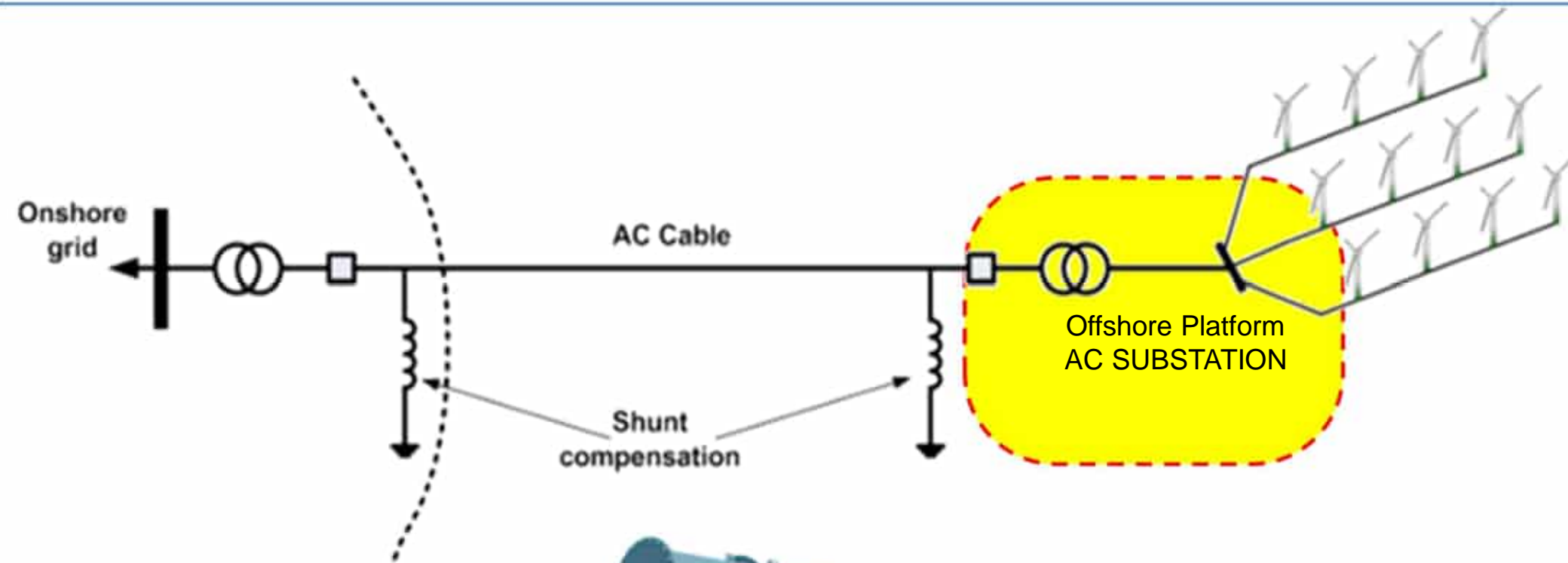
**General Arrangement
Wind Farm & Offshore Sub**

AECOM
6200 South Quebec Street Greenwood Village, CO 80111



REV	BY	DATE	REV	DATE	REVISIONS	BY	CHKR	DRAWING STATUS				Aditado para Presentacion		
								ISSUED	REV	DATE	SDE	PEM	DRN:	DATE:
								PRELIMINARY	A	04-25-24		AP	CHKD:	DATE:
								APPROVED FOR CONSTRUCTION						
								NOT APPROVED FOR CONSTRUCTION UNLESS SIGNED & DATED. DESTROY ALL PRINTS BEARING EARLIER DATE &/OR REV.NO.				SCALE:	NTS	

Long distance submarine cables have high losses and can generate significant VARs necessitating reactors to control power factor.



Reactor

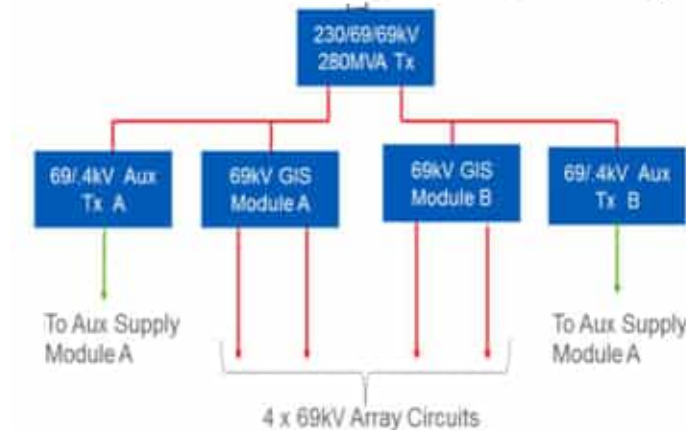
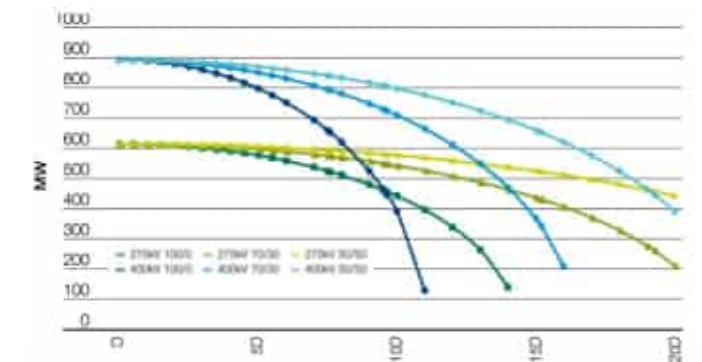


Transformer



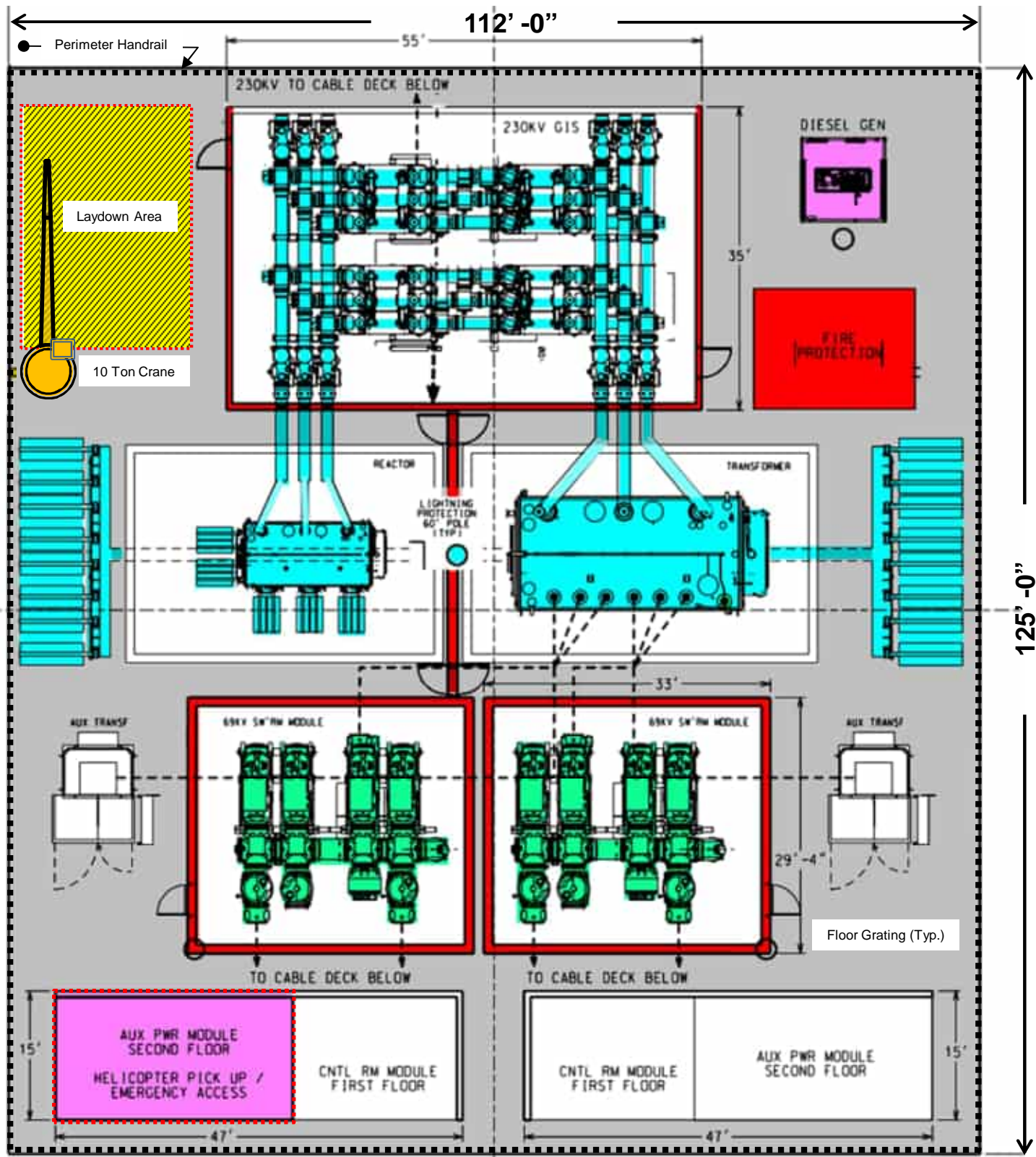
Transmission Voltage (kV)	Critical Distance (km)
132	370
220	281
400	202

Critical distance is achieved when half of the reactive current produced by the cable is equal to nominal current



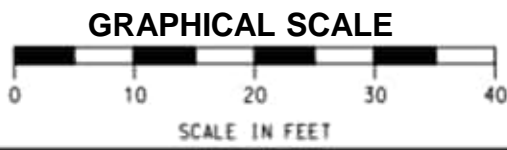
Atlantic Wind Connection (AWC)
230kV/69kV Substation
Offshore Platform

REVISION APPROVAL RECORD				REV	REV	DATE	REVISIONS	BY	CHKR	DRAWING STATUS				Aditado para Presentacion		
DISCIPLINE	BY	DATE	DISCIPLINE	BY	DATE					ISSUED	REV	DATE	SDE	PEM	DRN:	DATE:
ARCH.			MECHANICAL							PRELIMINARY	A	04-25-24		AP	CHKD:	DATE:
CIVIL			NUCLEAR													
ELECTRICAL			PIPING													
ENVIRON.			PROCESS							APPROVED FOR CONSTRUCTION						
GEN. ARRANG.			QA / QC													
HVAC			STRUCTURAL													
I & C										NOT APPROVED FOR CONSTRUCTION UNLESS SIGNED & DATED. DESTROY ALL PRINTS BEARING EARLIER DATE &/OR REV.NO.					SCALE: NTS	



Mayor Equipment Weight & Dimensions

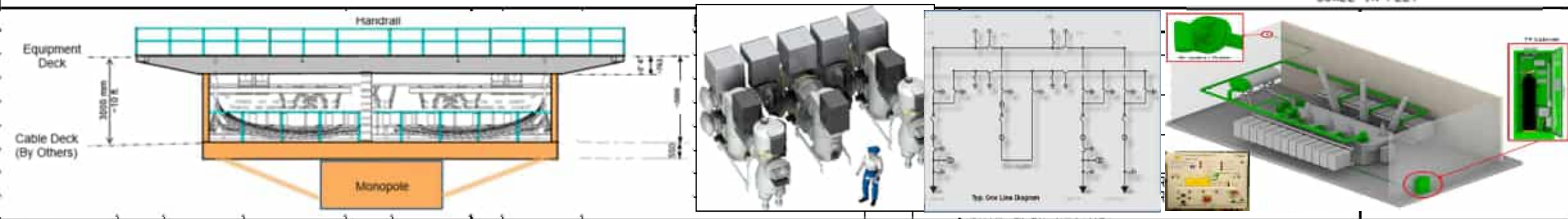
Item	Equipment Description	width		length		height		Weight US tons
		ft.	In	ft.	In	ft.	In	
1	230/69/69kV 280MVA Main transformer - tank	15	3	26	11	31	2	275.8
2	230/69/69kV 280MVA Main transformer - cooler	10	4	26	1	16	5	40.7
3	230/69/69kV 280MVA Main transformer cooler	10	4	26	1	16	5	40.7
4	230kV 60MVar reactor	15	9	36	1	20	4	98.2
5	Auxiliary transformer A	3	11	7	3	7	3	4.4
6	Auxiliary transformer B	3	11	7	3	7	3	4.4
7	"Sergi" fire suppression system skid	9	10	16	5	13	1	22.0
8	230 kV GIS Module	35	0	55	0	18	10	37.3
9	69 kV Switchroom Module A	33	0	29	4	18	10	33.1
10	69 kV Switchroom Module B	33	0	29	4	18	10	33.1
11	Control Room Module A	11	10	32	2	12	6	36.0
12	Control Room Module B	11	10	32	2	12	6	38.7
13	Auxiliary Power Module A	11	10	19	0	12	6	33.1
14	Auxiliary Power Module B	11	10	19	0	12	6	33.1
15	Diesel Generator Module	9	10	9	10	24	7	44.1
16	Service Crane (Boom 20-50 ft.)	25	0	5	0	15	0	5.0
17	Dump Tank (Accommodate 85 ton transf Oil)	10	0	10	0	40	0	15.0
	Contingency @ 10%							88.3
Total								883

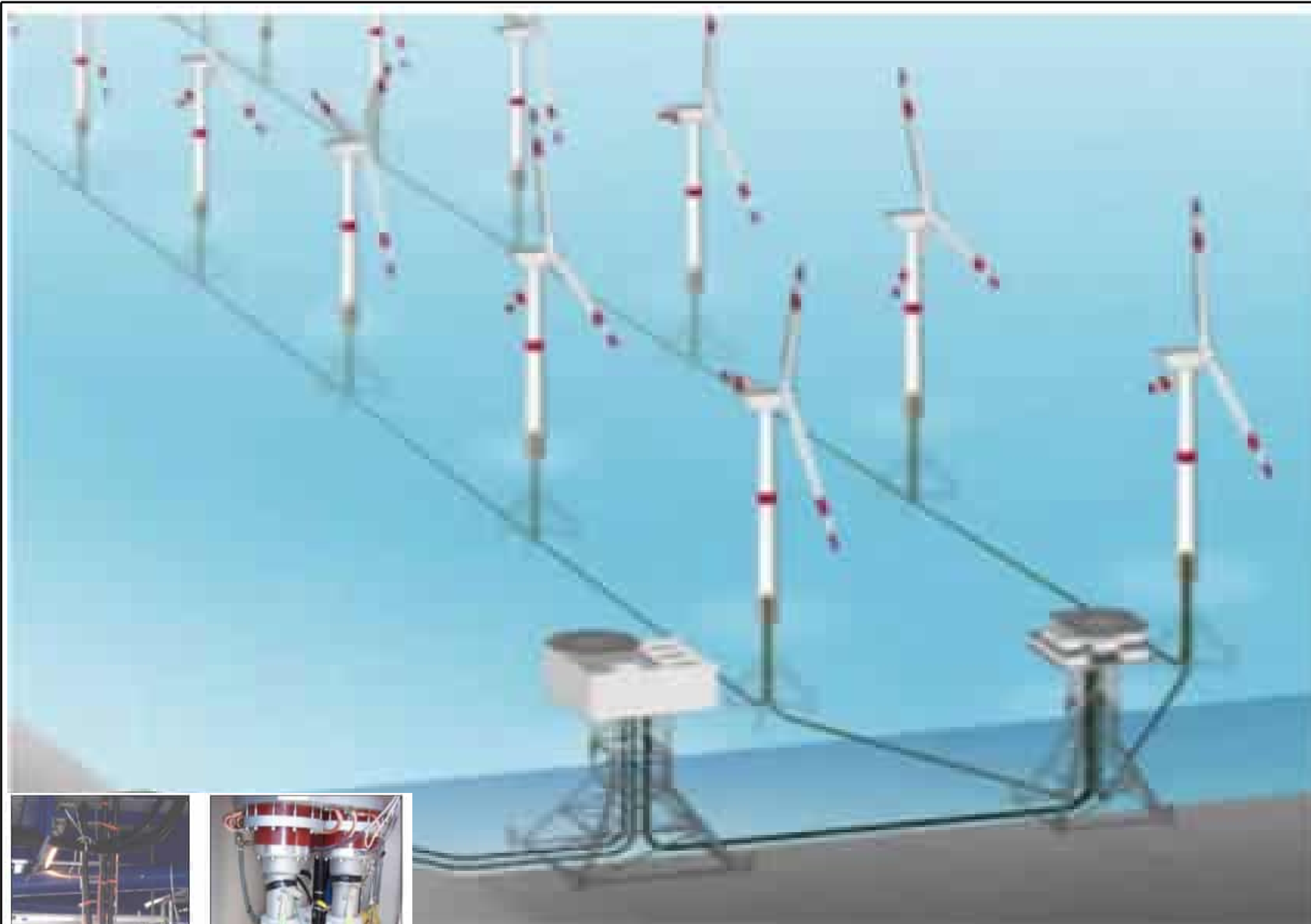


Atlantic Wind Connection (AWC)
230kV/69kV Substation
Offshore Platform

Equipment Deck BOM & Platform General Arrangement

AECOM
6200 South Quebec Street Greenwood Village, CO 80111

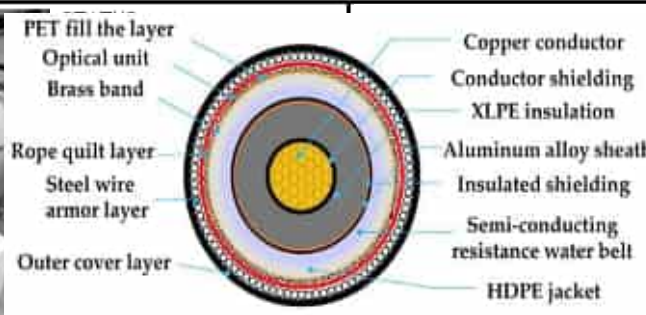




Jacket Foundation



Monopile up to ~630 MW




 Atlantic Wind Connection (AWC)
 230kV/69kV Substation
 Offshore Platform

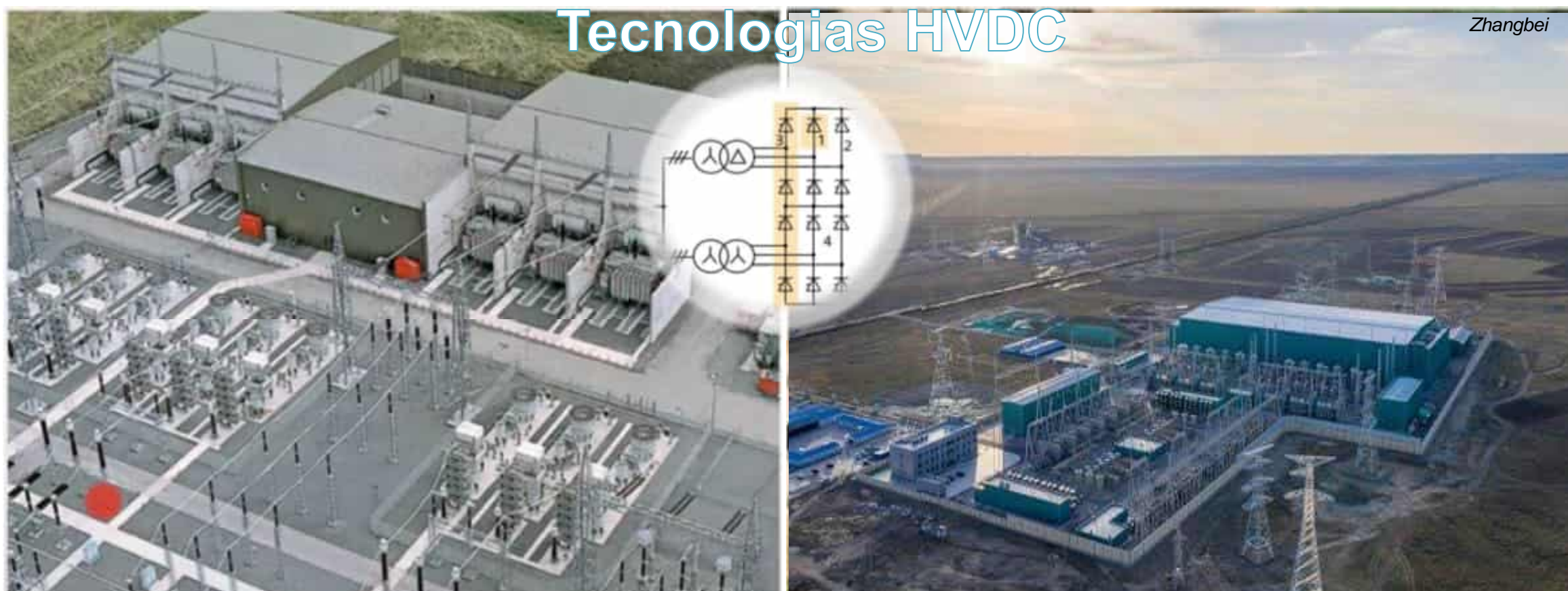
Offshore AC Substation & Wind Generators

AECOM

6200 South Quebec Street Greenwood Village, CO 80111

Tecnologías HVDC

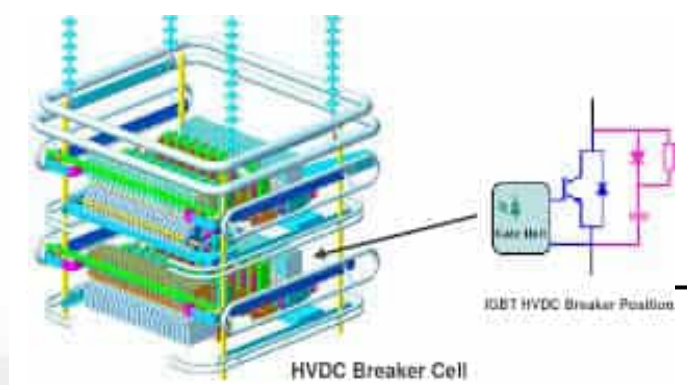
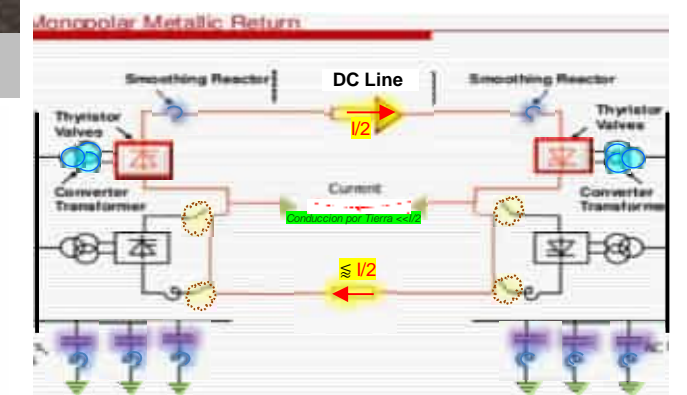
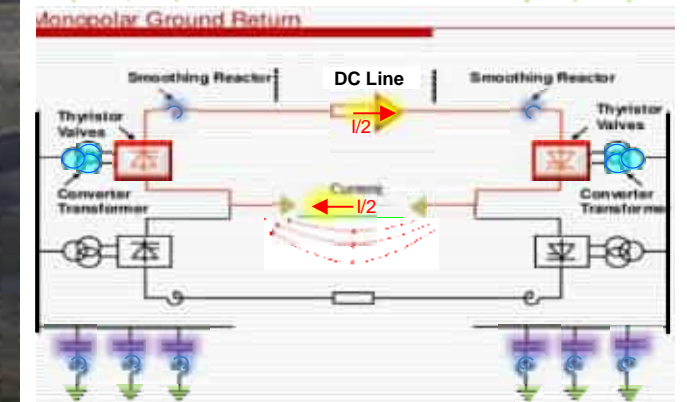
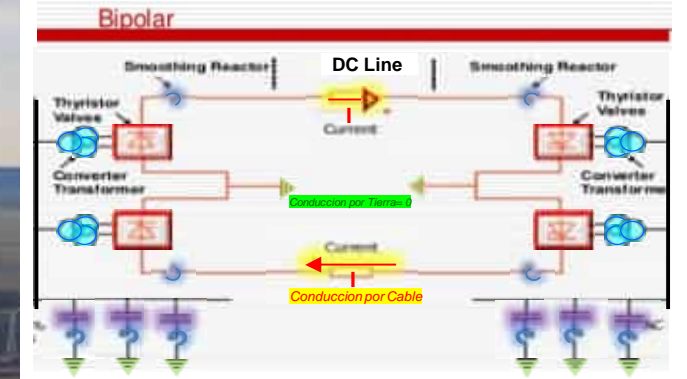
Zhangbei



HVDC Clasico –LCC- Tiristores – 4,000 a 8,000 MW & $\leq 1,100$ kV

HVDC VSC – Gate Bipolar Transistors 500 - 3,000 MW & $\leq \pm 535$ kV

CONFIGURACIONES HVDC



Evolucion de la Tecnologia HVDC

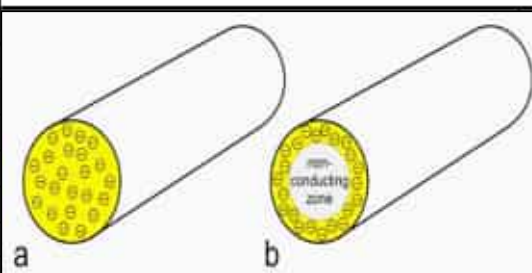
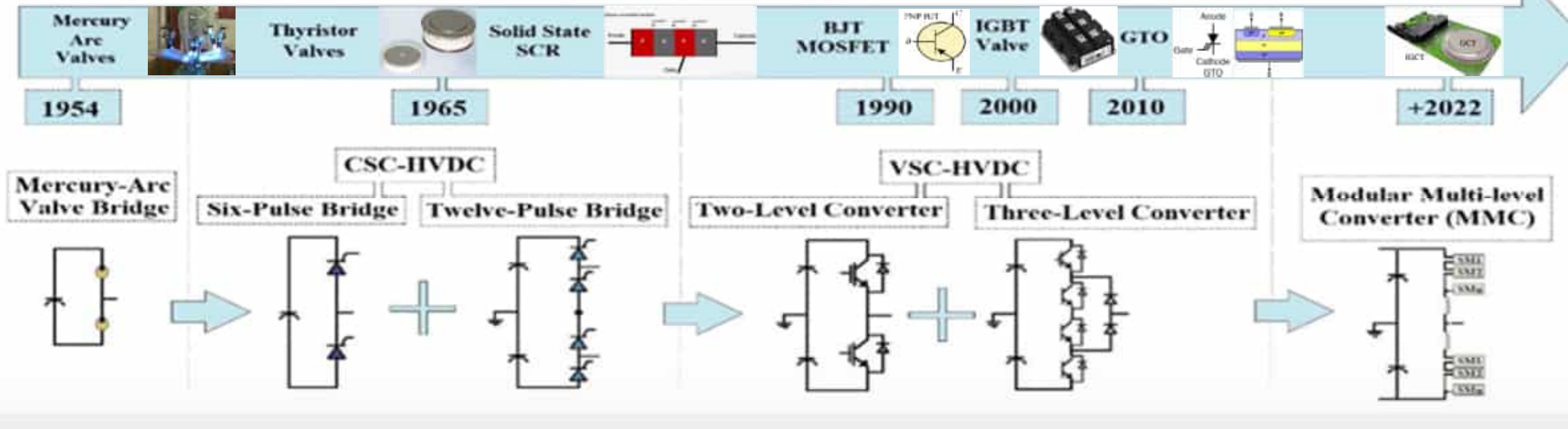
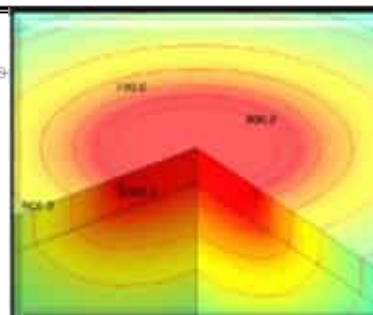
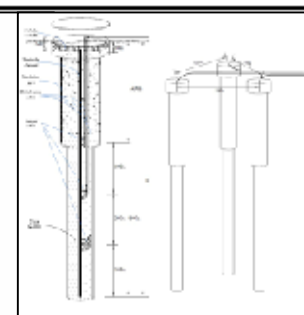
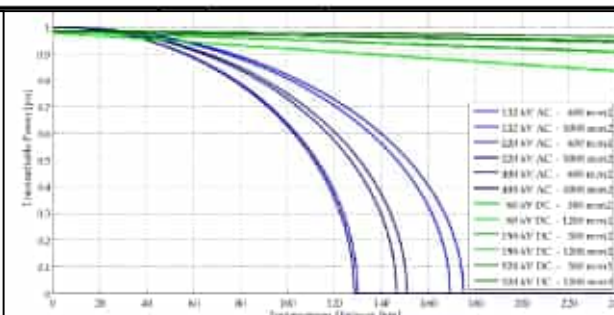
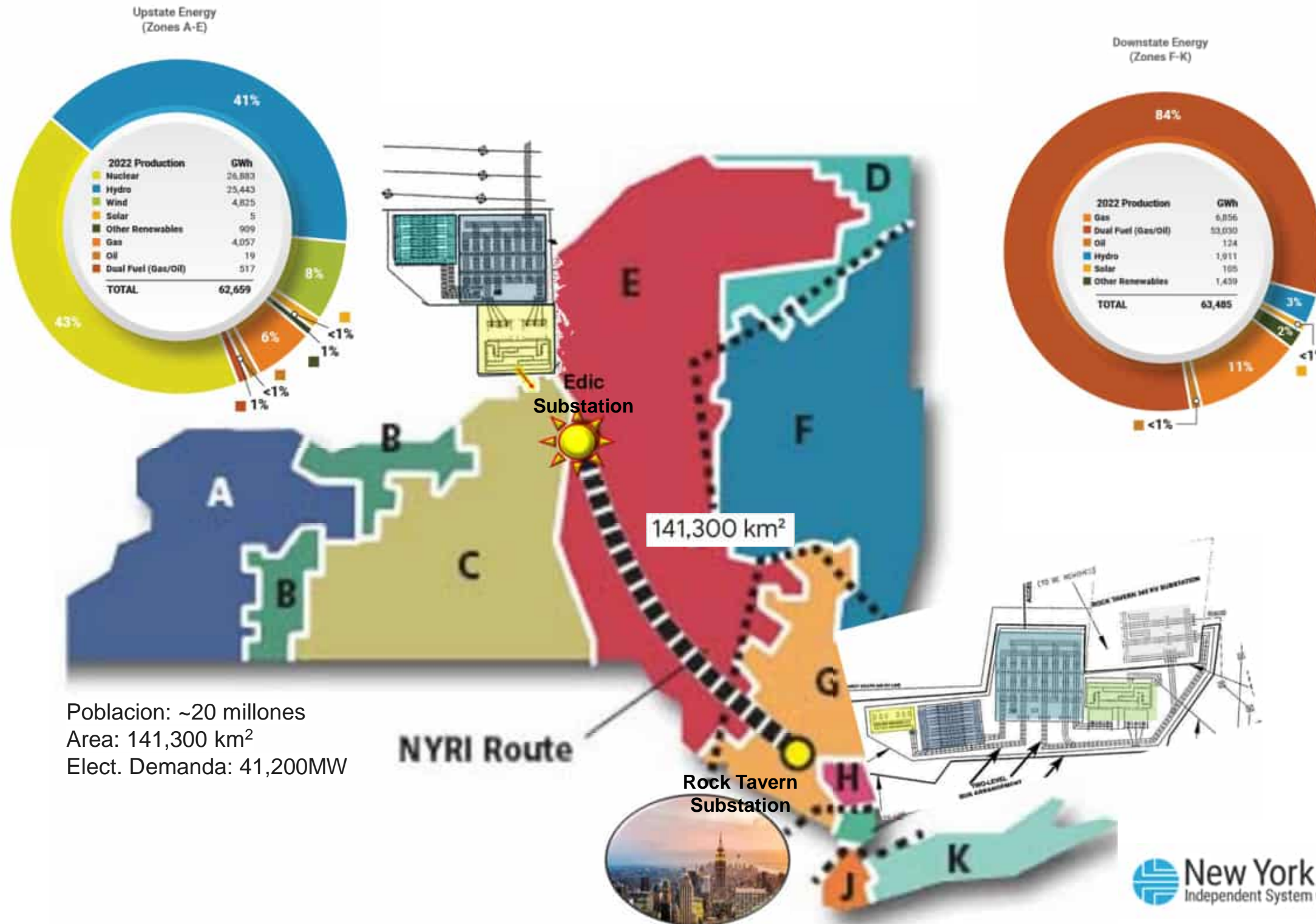


Figure 1 - DC (a) and AC (b) flow in a conductor: the skin effect



Comparacion con los Tipos De Tegnologia de HVDC

HVDC LCC - NY Regional Interconnection (NYRI), 1200MW, 300 km de Lineas @ ±400 kV



Poblacion: ~20 millones
 Area: 141,300 km²
 Elect. Demanda: 41,200MW

DESCRIPCION GENERAL

- **Capacidad HVDC:** 1200MW, ±400kV dc, estaciones convertidoras bipolares interconectando dos empresas electricas, National Grid y Central Hudson Gas & Elect.
- **Typo de linea:** Hibrido con cable soterrado y aereo de 190 millas (305 kms).
- **Costos:** US\$2.1 Billion (2011)
- **Localizacion:** Norte del Estado de NY (Oneida Cty) donde hay abundante energia al suroested proximo a la ciudad de NY con alta demanda y buenos precios.
- **Proposito:** Aliviar las limitaciones del corredor de transmision *aprovechando la controlabilidad del flujo de potencia en HVDC para circunvalancear el congestionado corredor AC*
- **Tarifa Electrica:** Reduccion costo de los consumidores 6%, incrementar margen de ganancias de los generadores y aumentar los ingresos asociados con la congeston.

NYISO – Beneficios Economicos - HVDC

NYISO Annual (M\$)	Base Case No HVDC	With HVDC	Benefit (M\$)
Consumer Payment	9300.53	9290.81	9.72
Producer Net Profit	2573.81	2601.25	27.45
Congestion Cost	148.20	137.31	-10.89
Total NYISO Benefit			26.28

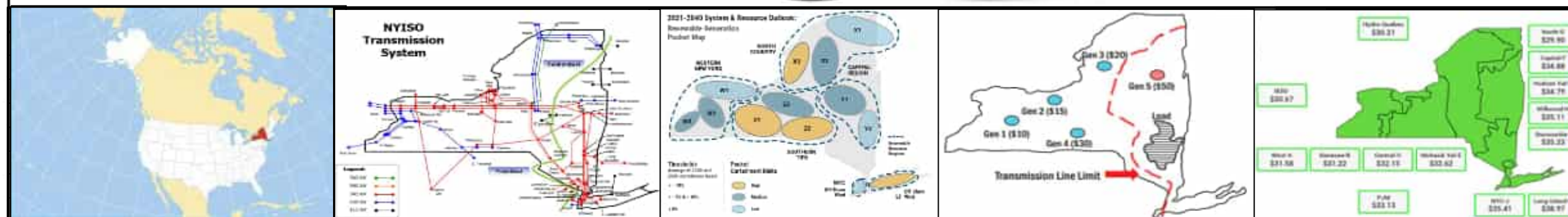
NYISO – Beneficios Economicos - HVAC

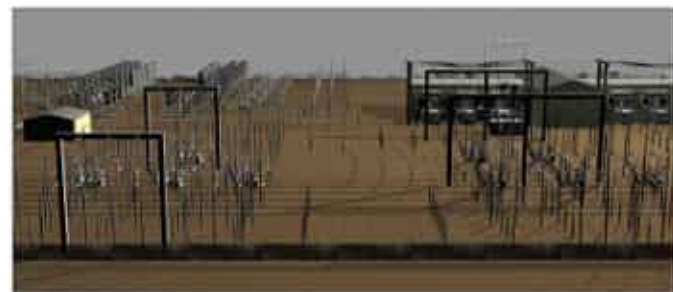
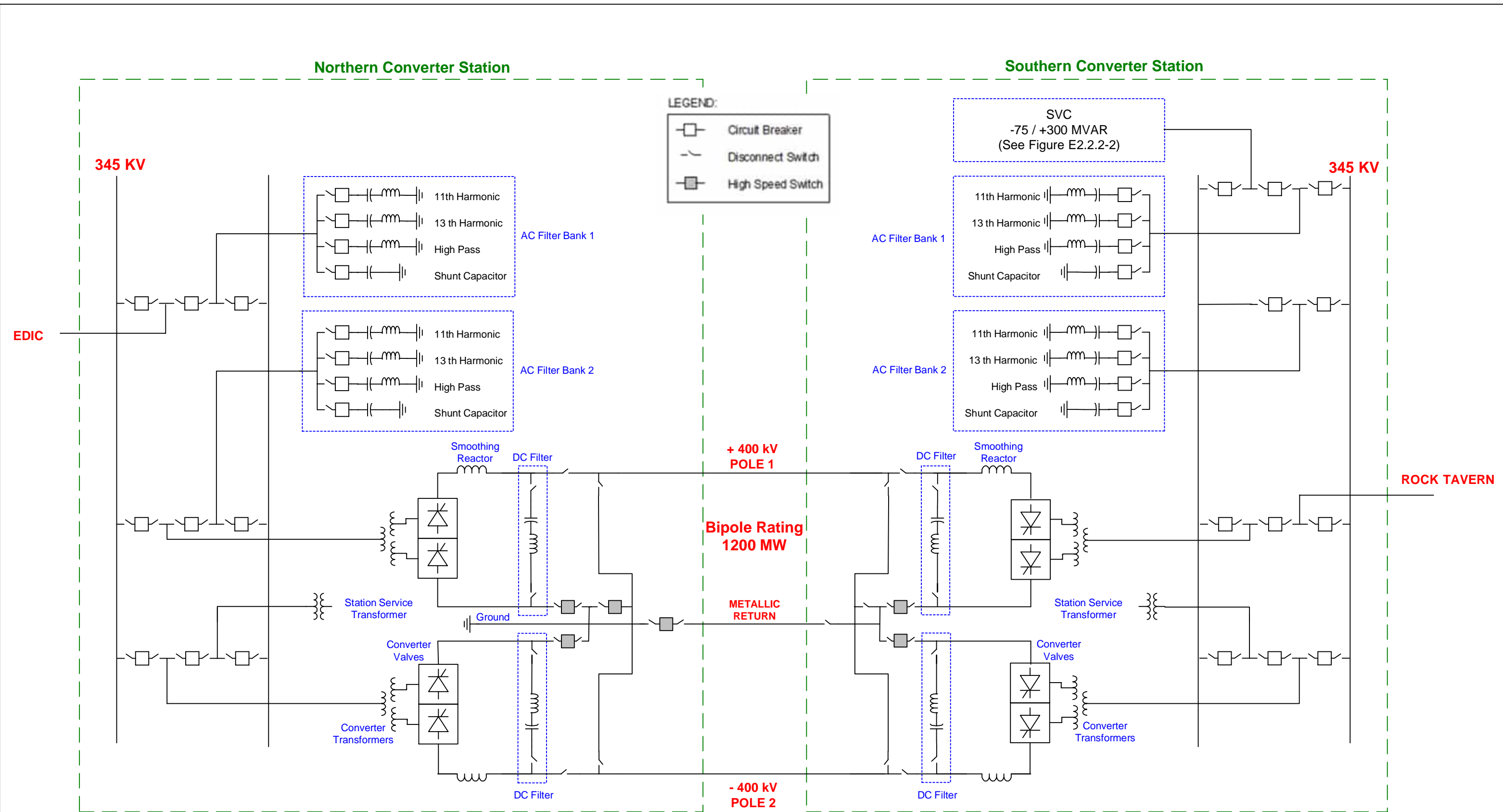
NYISO Annual (M\$)	Base Case No HVDC	With AC	Benefit (M\$)
Consumer Payment	9300.53	9298.99	1.54
Producer Net Profit	2573.81	2588.67	14.86
Congestion Cost	148.20	141.97	-6.22
Total NYISO Benefit			10.18

LBMP = Energy + Loss - Congestion



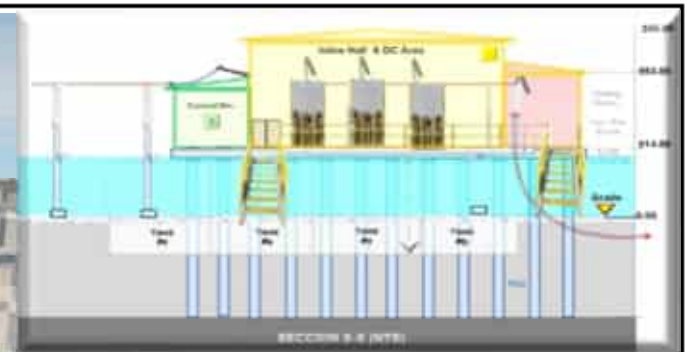
Datos Generales & Beneficios del Proyecto





New York Regional Interconnection
DC System
Single Line Diagram

Beacon Wind HVDC- NY ~US\$2.5B

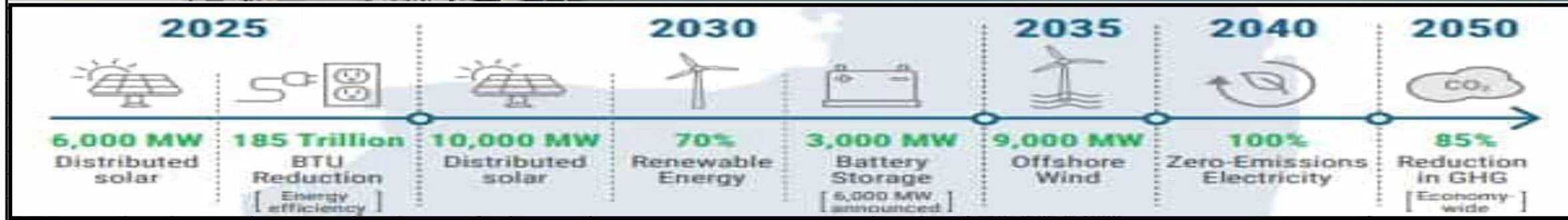


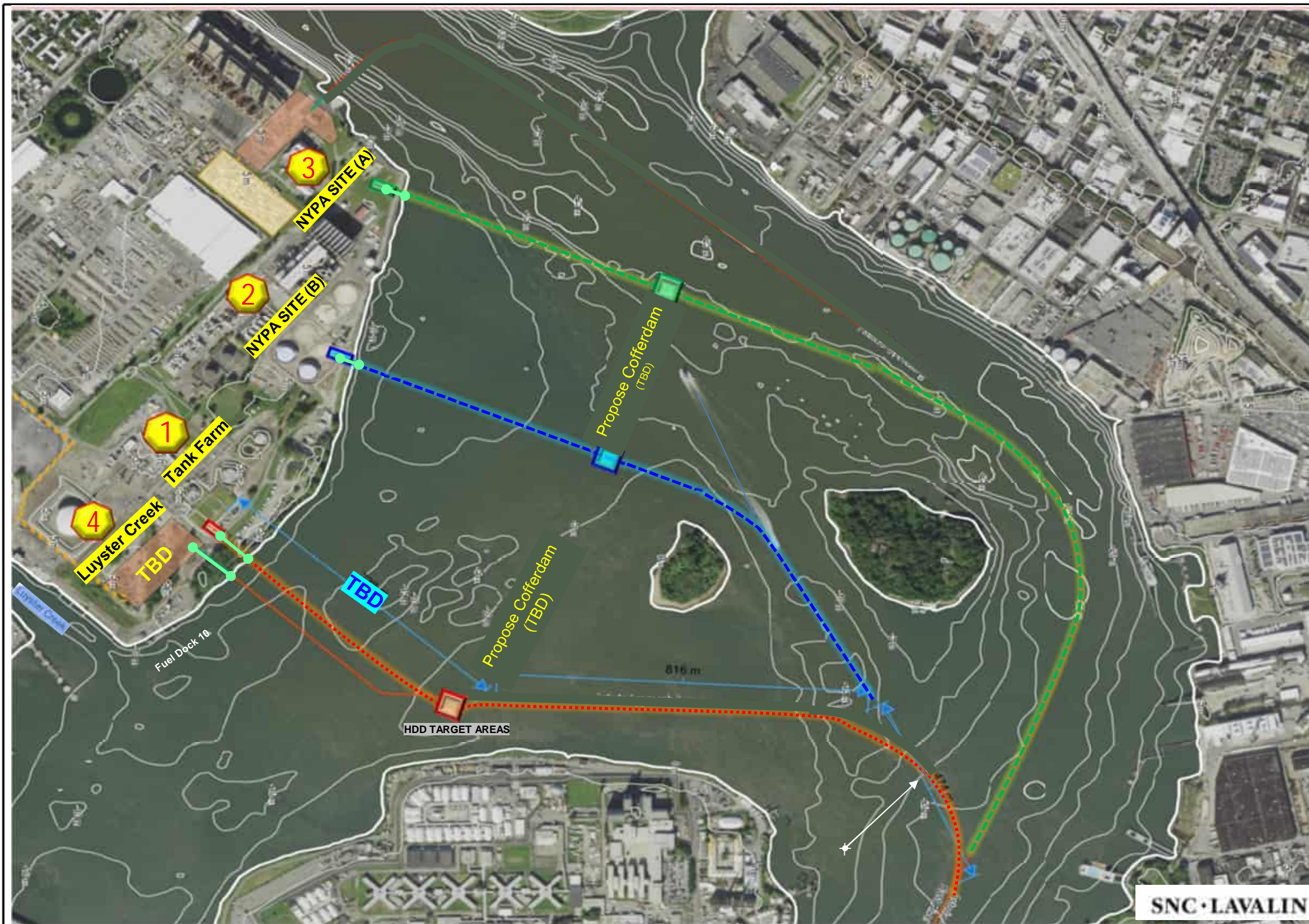
Characteristic	Rating
Rated Power	1,300 MW
Rated Voltage	± 320 kV
Rated Current	2,031 A
Insulation	XLPE
Insulation temperature	
Continuous operating	70°C
Emergency operation	N/A
Water Depth (m)	35 to 65
Average Sea water temp (°C) at 30 m water depth	16
Cable burial depth offshore (m)	1.82 m (6 ft)
Cable Installation method	Cable buried in trench
Seabed Soil resistivity (K.m/ W)	0.7
Min Max ambient temp (Cable in J-tube)	27 / -19
Solar Radiation on J tube (W / m2)	500
Landfall Installation In HDD,	max depth up to 25 m
Landfall resistivity (K.m/ W)	0.9
Ground temperature at HDD <small>Dependent on chosen HDD profile.</small>	To be evaluated.
Onshore cable burial depth (m)	1.5
Ground temp at 1.5 m burial depth (°C)	20
Onshore soil Thermal resistivity (K.m/ W)	1.2
Offshore Ambient Air temp (°C) Max/ Min	27 / -19



Project EQUINOR CABLE ROUTING PROJECT

NYP&A 3D RENDERING 1
Base Design 4-1φ Transf & AIS Bkrs





Project EQUINOR CABLE ROUTING PROJECT

Conceptual Submarine Cable



SKT No 24 of 12 Abril 25, 2024 REV. A

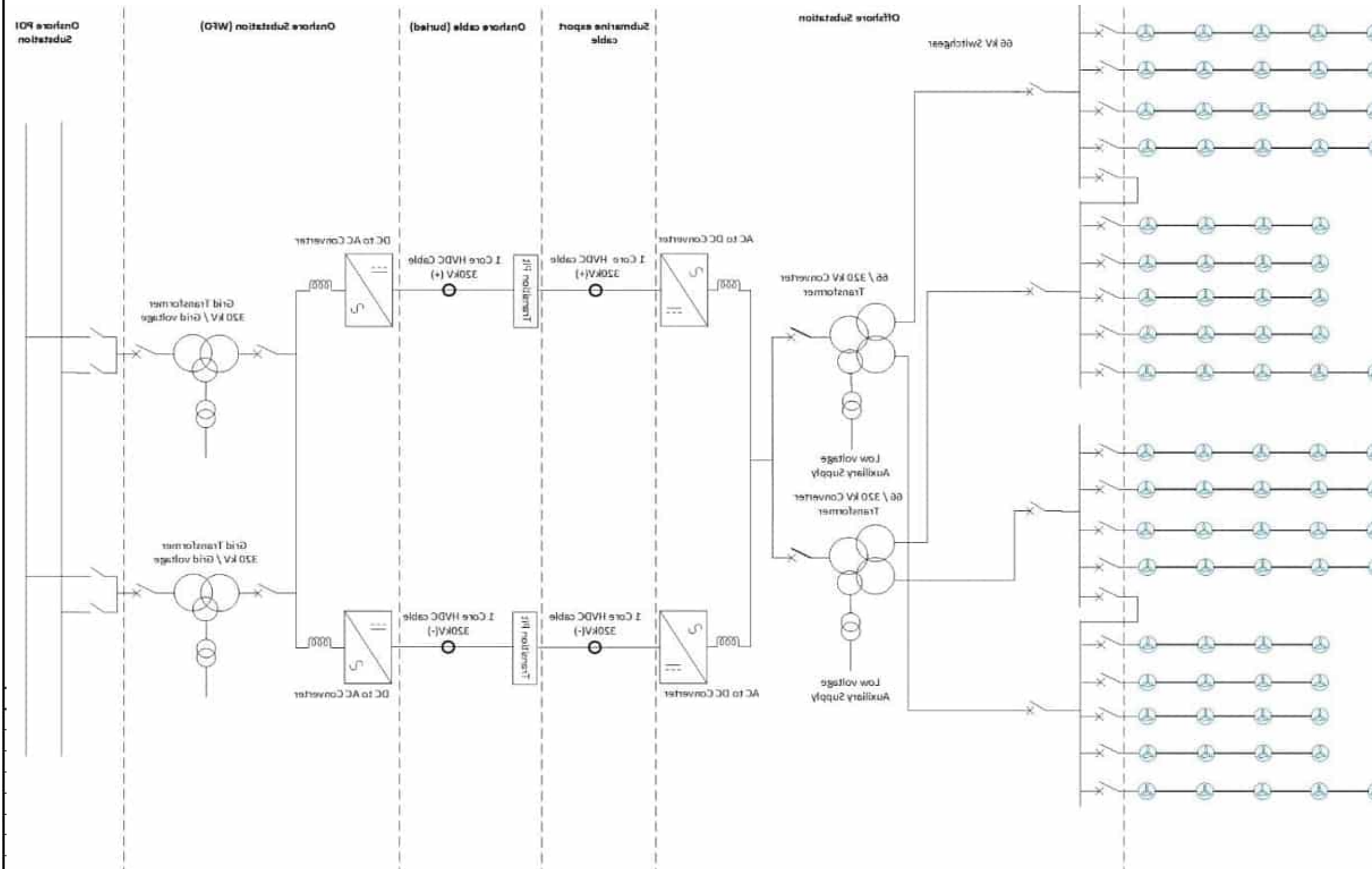
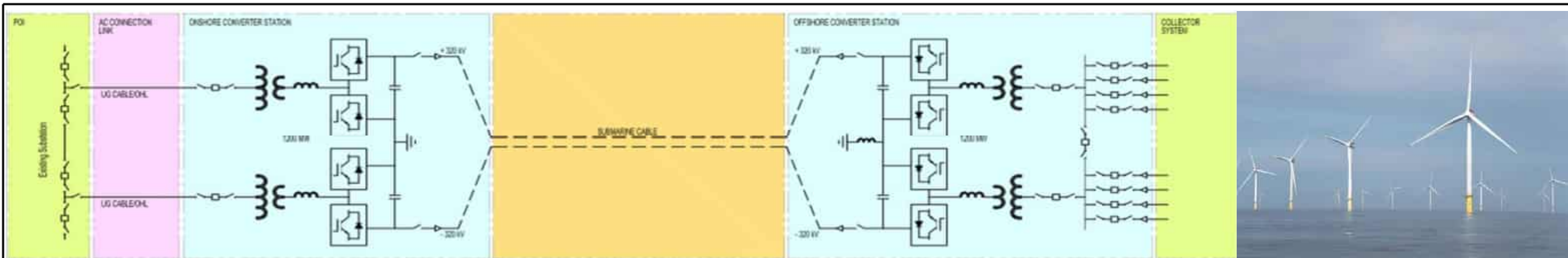
REVISION APPROVAL RECORD				REV	REV	DATE	REVISIONS	BY	CHKR	DRAWING STATUS				
DISCIPLINE	BY	DATE	DISCIPLINE	BY	DATE					ISSUED	REV	DATE	SDE	PEM
ARCH.			MECHANICAL							PRELIMINARY	A	04-25-24		AP
CIVIL			NUCLEAR											
ELECTRICAL			PIPING											
ENVIRON.			PROCESS							APPROVED FOR CONSTRUCTION				
GEN. ARRANG.			QA / QC											
HVAC			STRUCTURAL											
I & C														

SNC-LAVALIN

Aditado para Presentacion

SCALE: NTS

NOT APPROVED FOR CONSTRUCTION UNLESS SIGNED & DATED. DESTROY ALL PRINTS BEARING EARLIER DATE &/OR REV.NO.

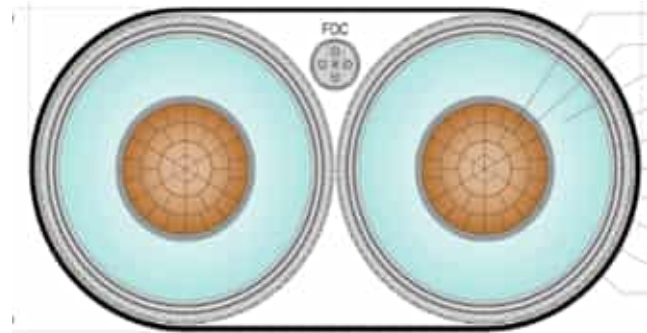


equinor

Project: EQUINOR CABLE ROUTING PROJECT

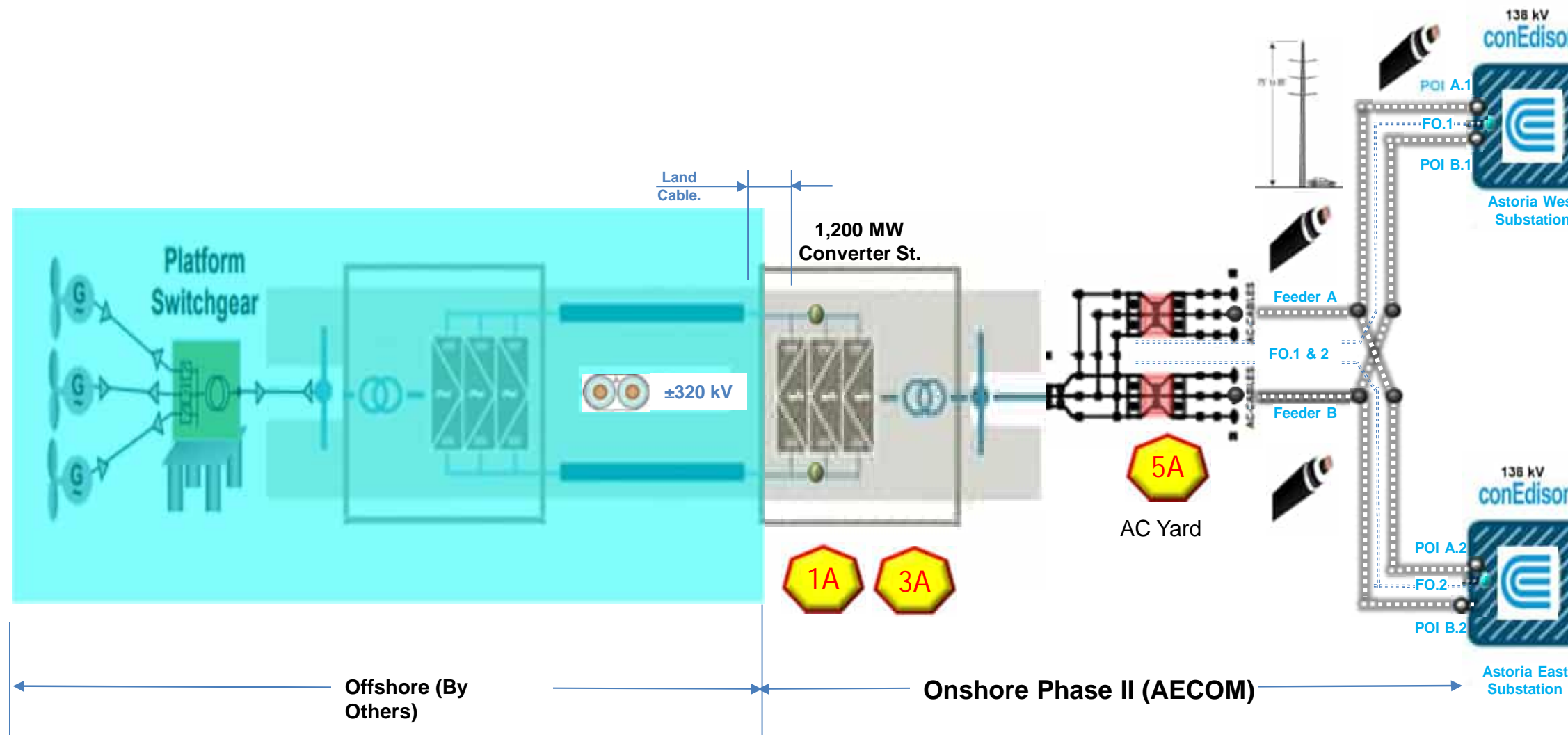
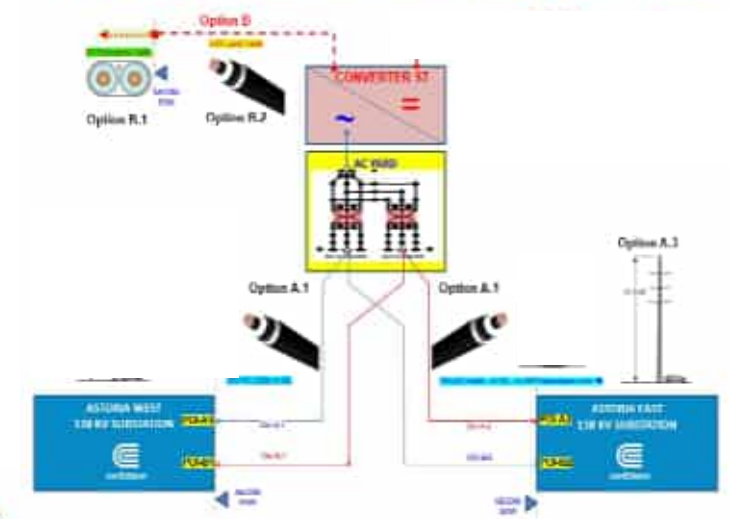
UNITED
Engineers & Constructors

SKT No 25 of 12 April 25, 2024 REV. A



3. Extend Submarine Cable

DC & AC INTERCONNECTING HV LINES



NOTE: POI locations & circ Bkrs. TBD



equinor

Project: EQUINOR CABLE ROUTING PROJECT

SIMMETRICAL MONOPOLE SYSTEM ONE LINE DIAGRAM

UNITED
Engineers & Constructors

SKT No 26 of 12 Abril 25, 2024 REV. A

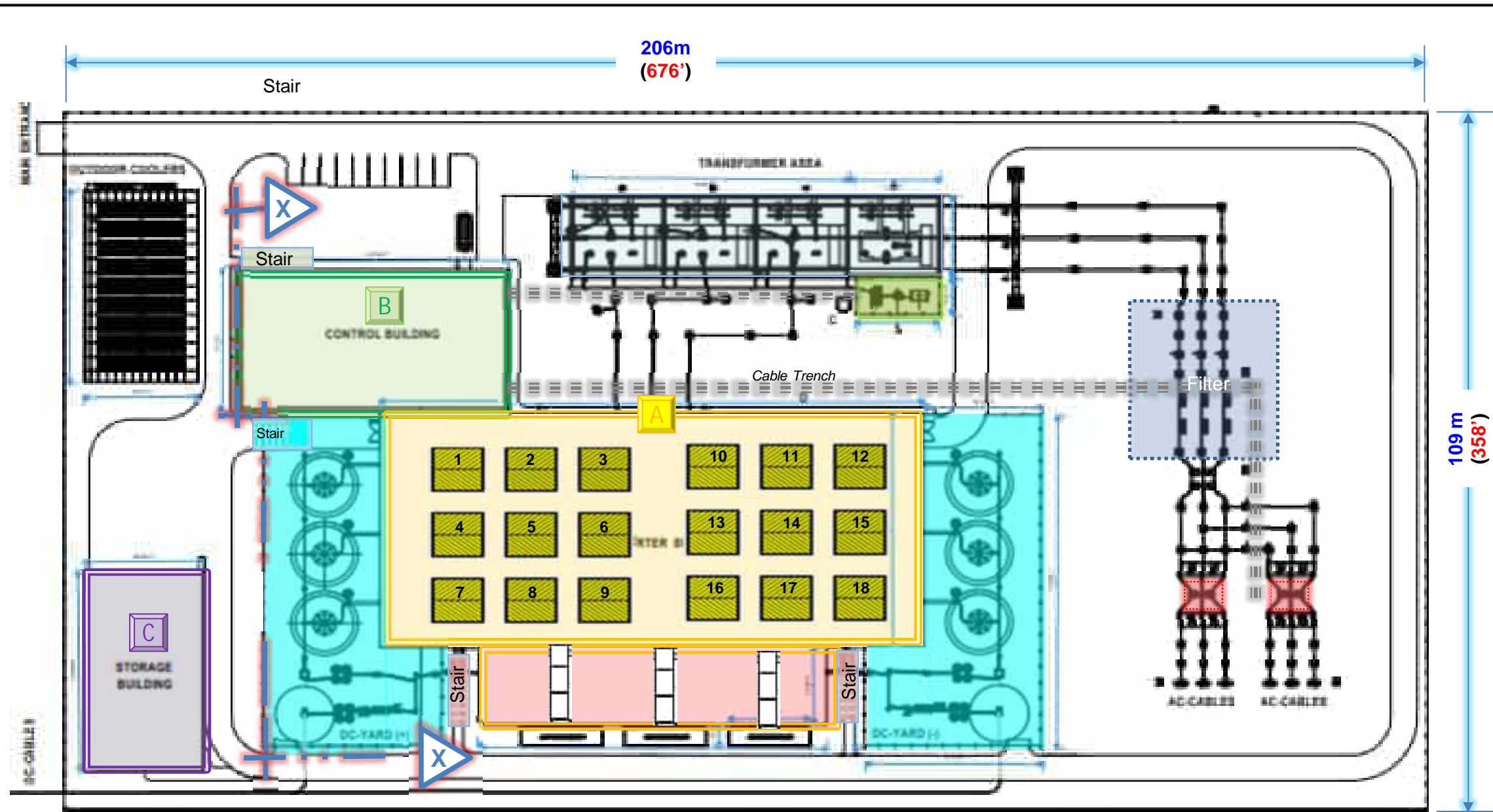
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ARCH.			MECHANICAL							PRELIMINARY	A	04-25-24		AP
CIVIL			NUCLEAR											
ELECTRICAL			PIPING											
ENVIRON.			PROCESS							APPROVED FOR CONSTRUCTION				
GEN. ARRANG.			QA / QC											
HVAC			STRUCTURAL											
I & C														

Aditado para Presentacion

DRN: DATE:

CHKD: DATE:

SCALE: NTS



PLAN VIEW

Task	Task Description	QTY	Dimensions (ft)		
			L	W	H
A BUILDING					
1.00	Converter Station	1	206	120	14
2.00	Cooling and Aux Pwr Rooms	1	172	30	14
3.00	Control Building	1	133	74	14
4.00	Storage Building	1	60	102	14
B DC HV EQUIPMENT :					
5.00	DC Air Cans Reactors & Equipment	3	54	120	12
a	AP over-mat	3			
b	Yieldable steel wall	3			
c	AC Cable terminations	3			
d	Single arrester	3			
e	Bus /Aux support structures	3			
C AC YARD HV EQUIPMENT :					
1	AC air group scaffolding	3			
a	Platform	1	151	43	14
b	Oil containment	4			
c	First rated fire wall	3			144x30'
2.00	Dead tank circuit breaker	2	15	15	14
3.00	Disconnect switch (4 leg structure)	2	0.75	0.75	14
4.00	H-Frame (2 leg foundations)	2	1	1	14
5.00	Bus support (2 foundation)	24	0.75	0.75	14
6.00	Bus support 3 phase (2 found, 11 strut)	11	0.75	0.75	14
7.00	Lighting mast (monopole)	6	1.5	1.5	30
8.00	Cable termination & surge arrester (2 terminations with 2 leg structure)	2	0.75	0.75	14
4.00	House Meter (1 & M) (2 leg structure)	2	0.75	0.75	14
D AC YARD HV EQUIPMENT AT POI (Astoria Substation East & West) :					
1.00	Cable termination & surge arrester (2 terminations with 2 leg structure)	4	0.75	0.75	14
2.00	House Meter (1 & M) (2 leg structure)	4	0.75	0.75	14
3.00	Interconnect with existing busbar	LoL			
E AC LV COMPONENTS					
1.00	Station Service Transformer (Bus Mount)	2	12	12	14
2.00	Diesel generator & load bank	1	15	7.5	14
3.00	Trench (excavate & backfill)	575'	2	4	
4.00	Manhole/Handhole	2	8	12	
5.00	Lighting pole	4	1	23	
F FENCE & SECURITY EQUIPMENT :					
1.00	Pole for camera/horn & lights	8	0.75	0.75	20
2.00	Heavy security gate	1			10
3.00	Card reader	2	0.25	0.25	5
4.00	Bollards and misc. bollards	8	0.25	0.25	4
5.00	Perimeter fence & gates (10)	20x8			8
G MECHANICAL & WATER EQUIPMENT					
1.00	Cooler (HVAC Components)	1	57	93	24
2.00	Water tank (reservoir) in slab/piles	1	10	10	24

LEGEND:
A STAR POINT AREA
B EARTHING TRANSFORMER
C HVAC COOLERS
D SIDEWAY
E SPARE TRANSFORMER
F AC CABLE SEALING ENDS

No Towers: 3x 6 = 18*

* To be validated

DRAFT : 00, 2020-09-16

REF: SIEMENS LAYOUT

NOTES	* Platform to be elevated 14' above existing grade
AECOM Scope:	** Prepare the cost estimate for the below grade scope and extended up to the building floor, platform or equipment base elevated up to the flood level and include all steel support.
Reference:	The design criteria of this work follow the ConEdison standard practice for flood protection elevating equipment + 3 ft above the FEMA 100 year flood level.

REVISION APPROVAL RECORD						DRAWING STATUS					
DISCIPLINE	BY	DATE	DISCIPLINE	BY	DATE	REV	DATE	SDE	PEM	Aditado para Presentacion	
ARCH.			MECHANICAL			ISSUED				DRN:	DATE:
CIVIL			NUCLEAR			PRELIMINARY	A	04-25-24	AP	CHKD:	DATE:
ELECTRICAL			PIPING								
ENVIRON.			PROCESS			APPROVED FOR CONSTRUCTION					
GEN. ARRANG.			QA / QC			NOT APPROVED FOR CONSTRUCTION UNLESS SIGNED & DATED. DESTROY ALL PRINTS BEARING EARLIER DATE &/OR REV.NO.				SCALE:	NTS
HVAC			STRUCTURAL								
I & C											

equinor

Project: EQUINOR CABLE ROUTING PROJECT

1,230 MW -320 KV DC SYM MONOPOL CONVERTER STATION LAYOUT

UNITED
Engineers & Constructors

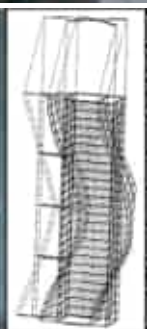
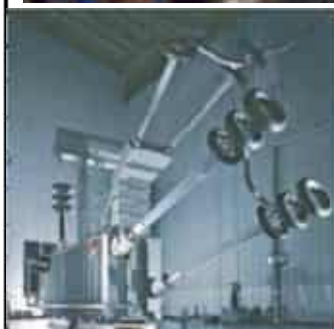
SKT No 28 of 12 Abril 25, 2024 REV. A

Cuarto de Valvulas Electronica



equinor 

Project: EQUINOR CABLE ROUTING PROJECT



REV	DATE	REVISIONS	BY	CHKR	DRAWING STATUS				Aditado para Presentacion	
					ISSUED	REV	DATE	SDE	PEM	DRN: DATE:
					PRELIMINARY	A	04-25-24		AP	CHKD: DATE:
					APPROVED FOR CONSTRUCTION					SCALE: NTS
NOT APPROVED FOR CONSTRUCTION UNLESS SIGNED & DATED. DESTROY ALL PRINTS BEARING EARLIER DATE &/OR REV.NO.										SKT No 29 of 12

Typ. Converter Valve Hall

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